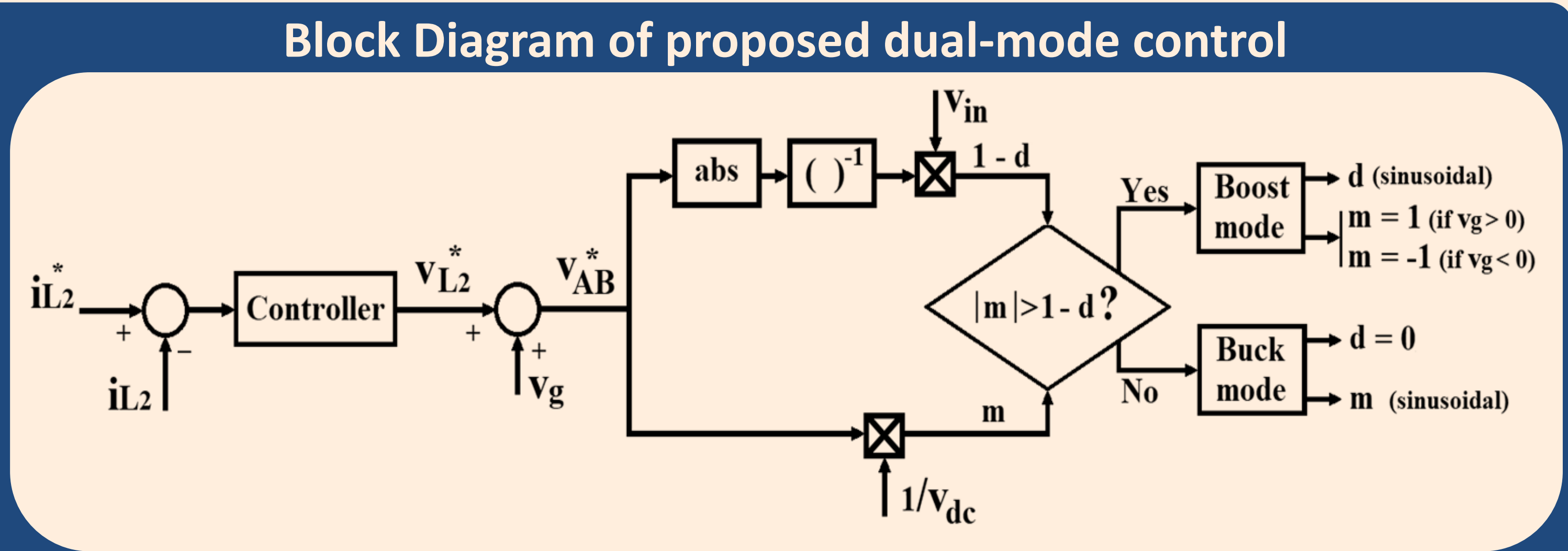
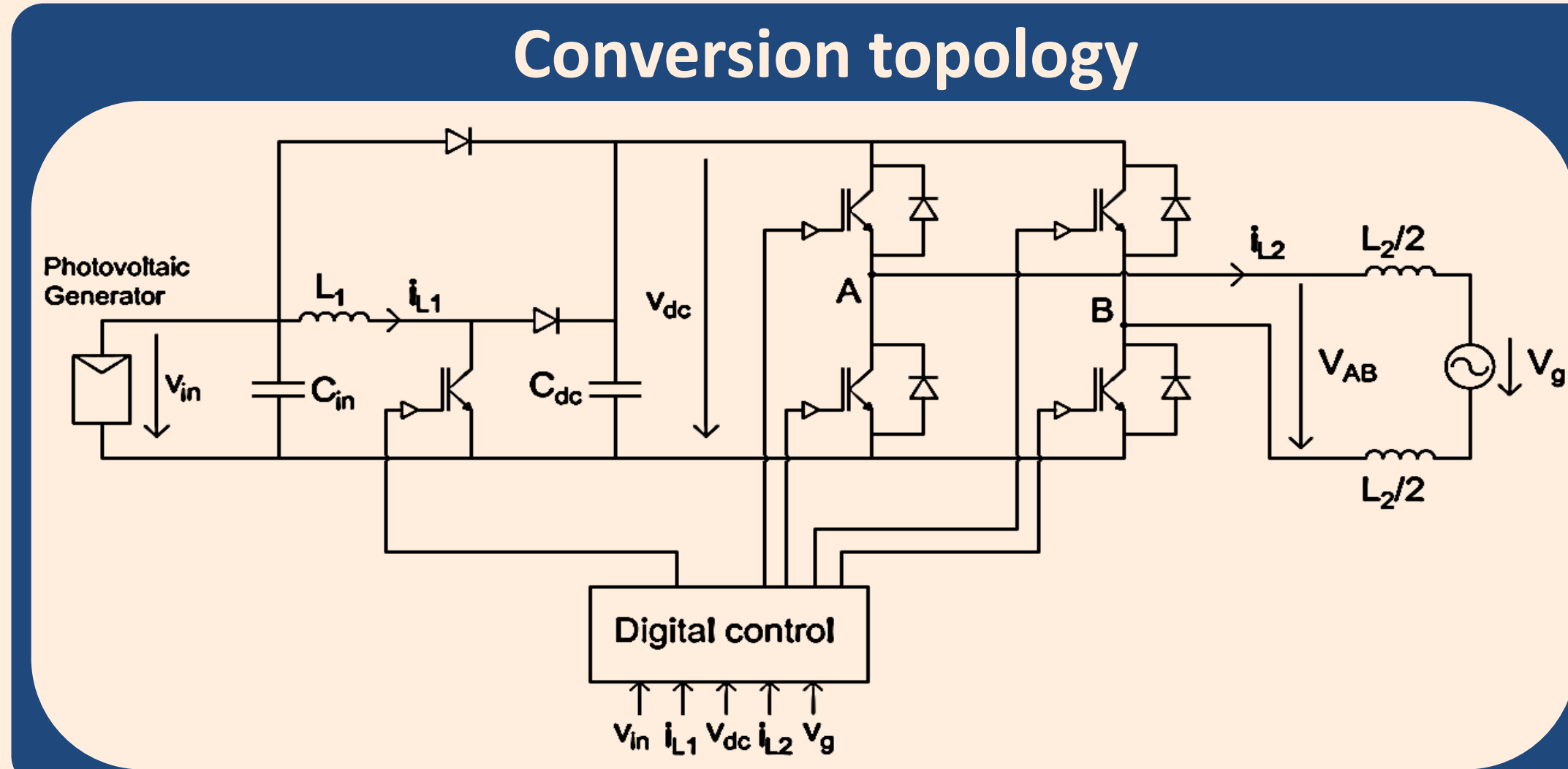


INTRODUCTION

- Dual-mode control methods for two-stage inverters have been widely analysed because of their high efficiency.
- Their main weak point is the abrupt transition between modes, affecting grid current quality.
- By applying suitable feed-forward compensations, the paper proposes a dual-mode soft-transition control method with universal controller for current control loop.



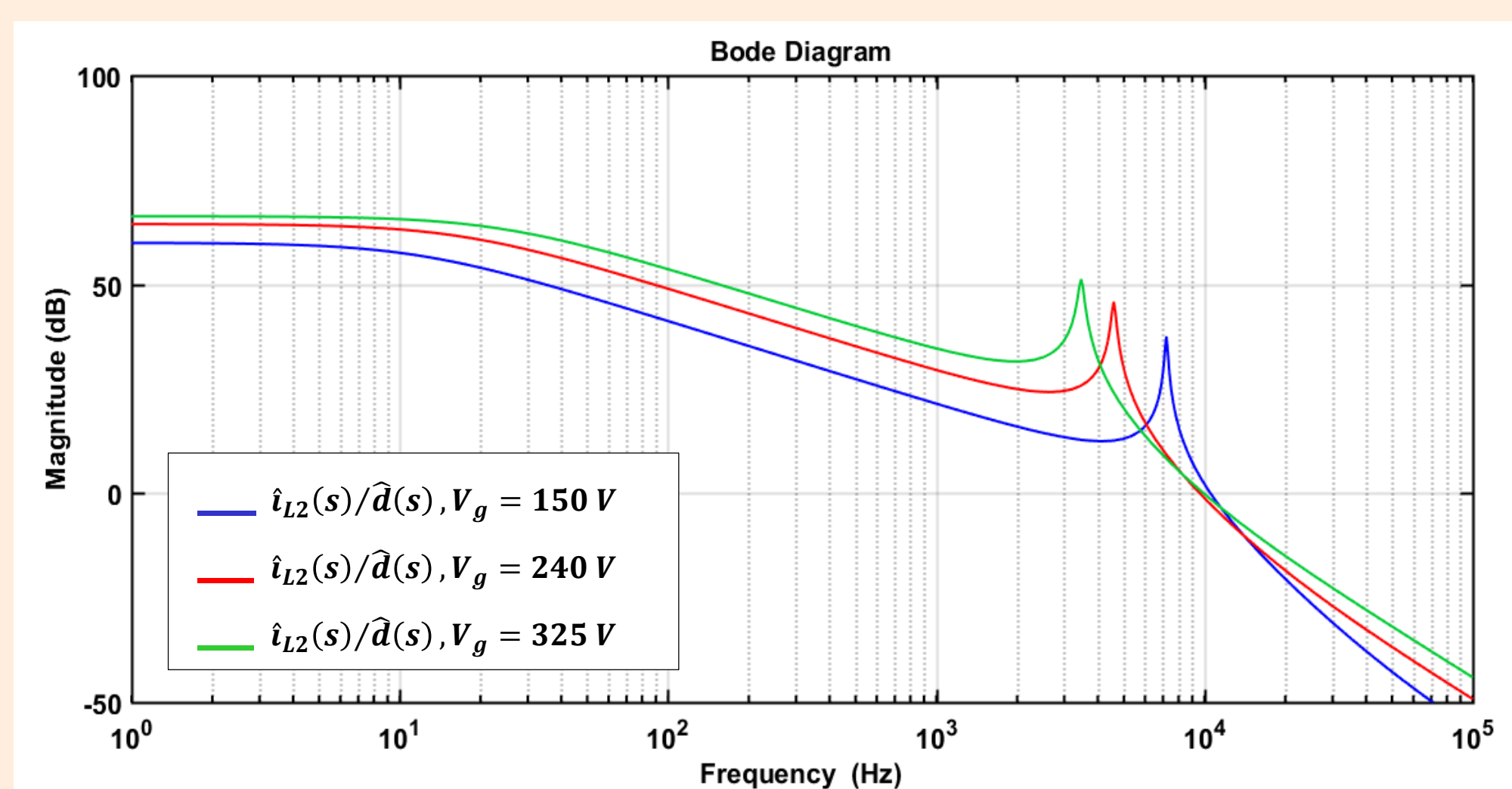
CURRENT CONTROL LOOP DESIGN

▪ Buck mode: $\hat{i}_{L2}(s) = \frac{1}{L_2 \cdot s + R_2} \approx \frac{1}{L_2 \cdot s}$

▪ Boost mode: $\hat{i}_{L2}(s) = \frac{-L_1 I_{L1} s - R_1 I_{L1} + V_{dc} (1-D)}{L_1 C_{dc} L_2 s^3 + (L_2 R_1 + L_1 R_2) C_{dc} s^2 + (C_{dc} R_1 R_2 + L_2 (1-D)^2 + L_1) s + R_1 + R_2 (1-D)^2} \hat{d}(s)$

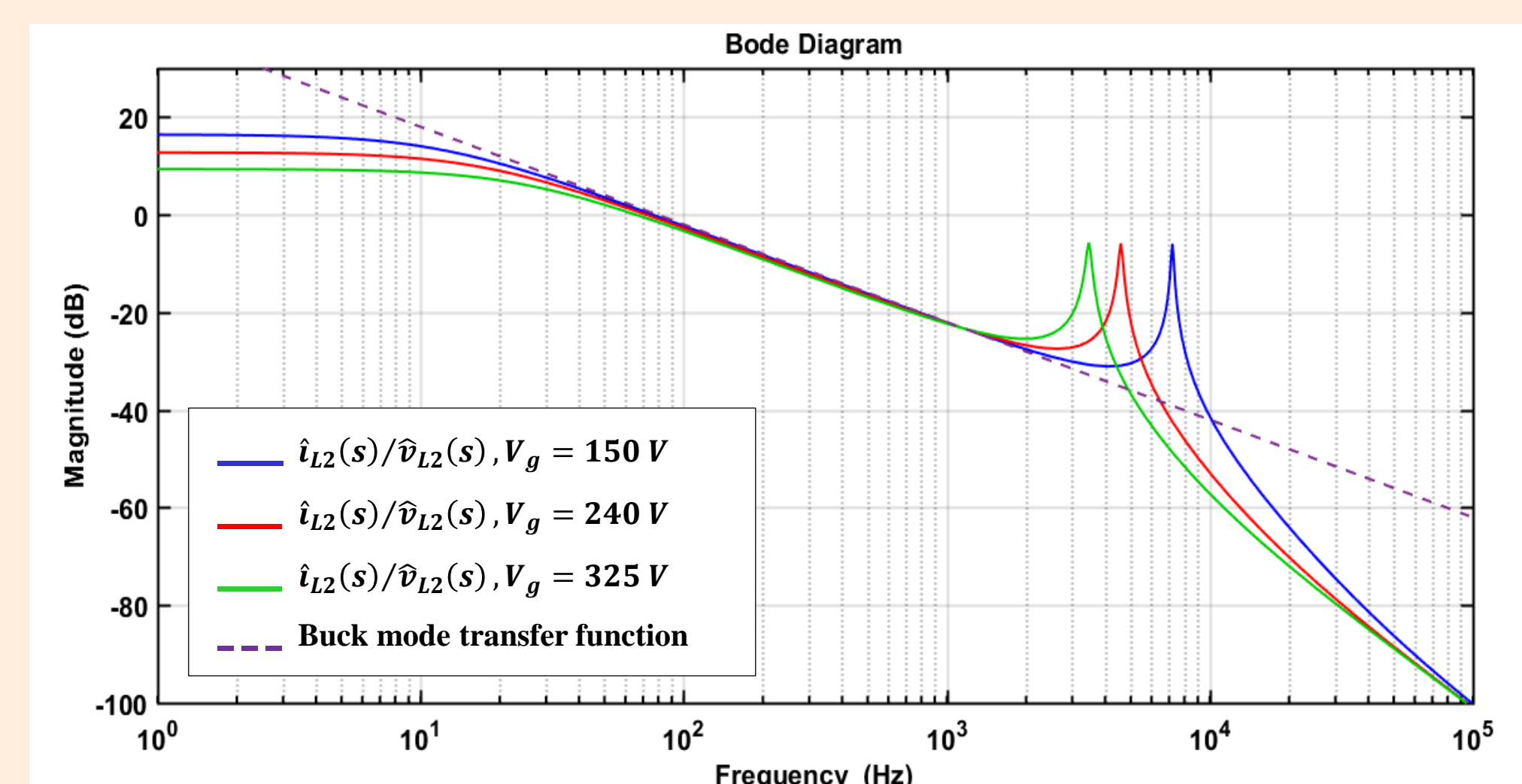
In **Buck mode**, control-to-grid current plant is a **first-order minimum phase system**.

In **Boost mode**, control-to-grid current plant is a **third-order system** with both resonance and magnitude operating-point dependent.



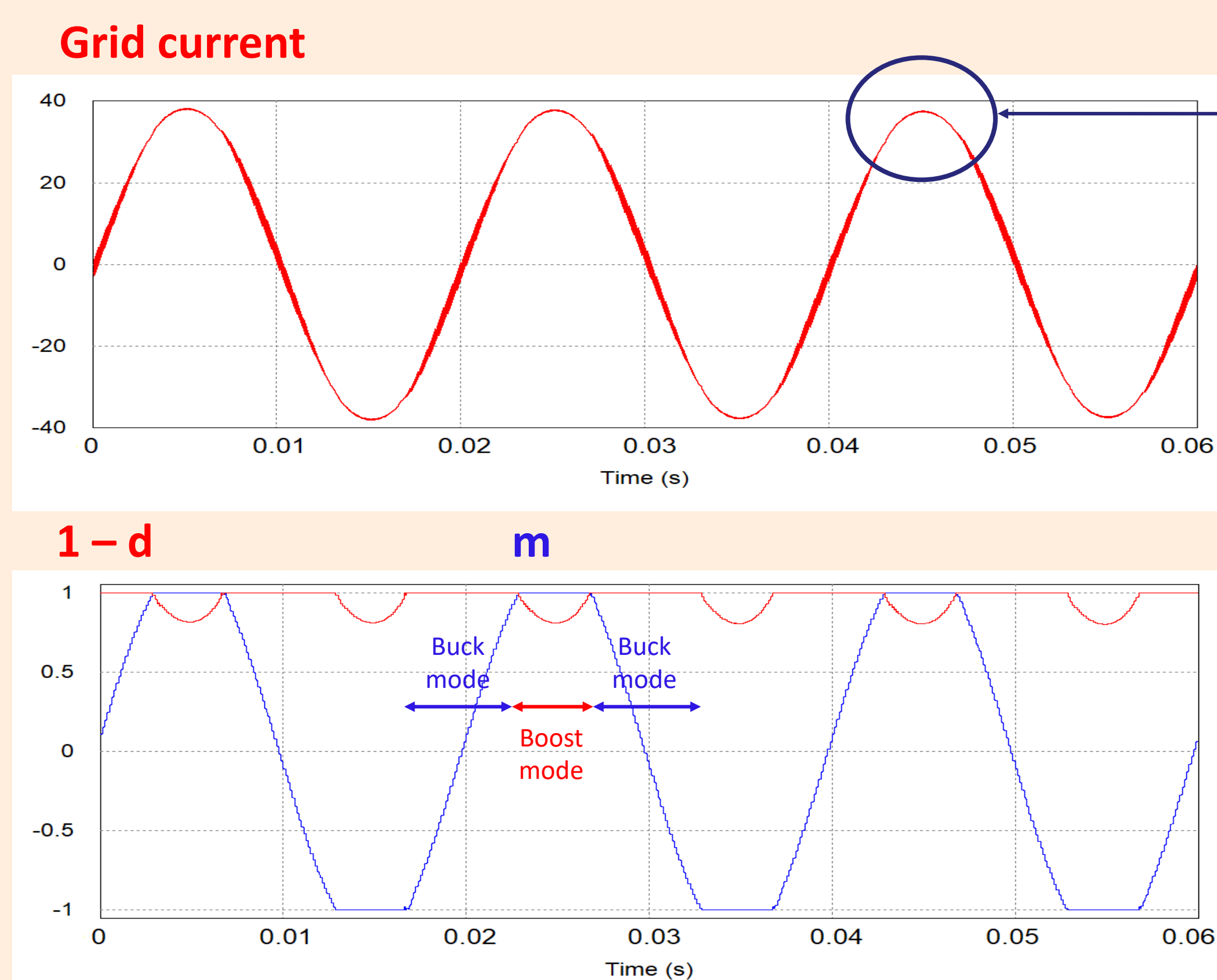
Peak resonance and variable magnitude affect control feasibility.

Applying proposed feed-forward compensations



$$\hat{i}_{L2}(s) = \frac{-L_1 I_{L1} (1-D) s / V_{dc} - R_1 I_{L1} (1-D) / V_{dc} + (1-D)^2}{L_1 C_{dc} L_2 s^3 + (L_2 R_1 + L_1 R_2) C_{dc} s^2 + (C_{dc} R_1 R_2 + L_2 (1-D)^2 + L_1) s + R_1 + R_2 (1-D)^2} \hat{d}(s) \approx \frac{1}{L_2 \cdot s} \text{ in } f_c \text{ range}$$

SIMULATION RESULTS



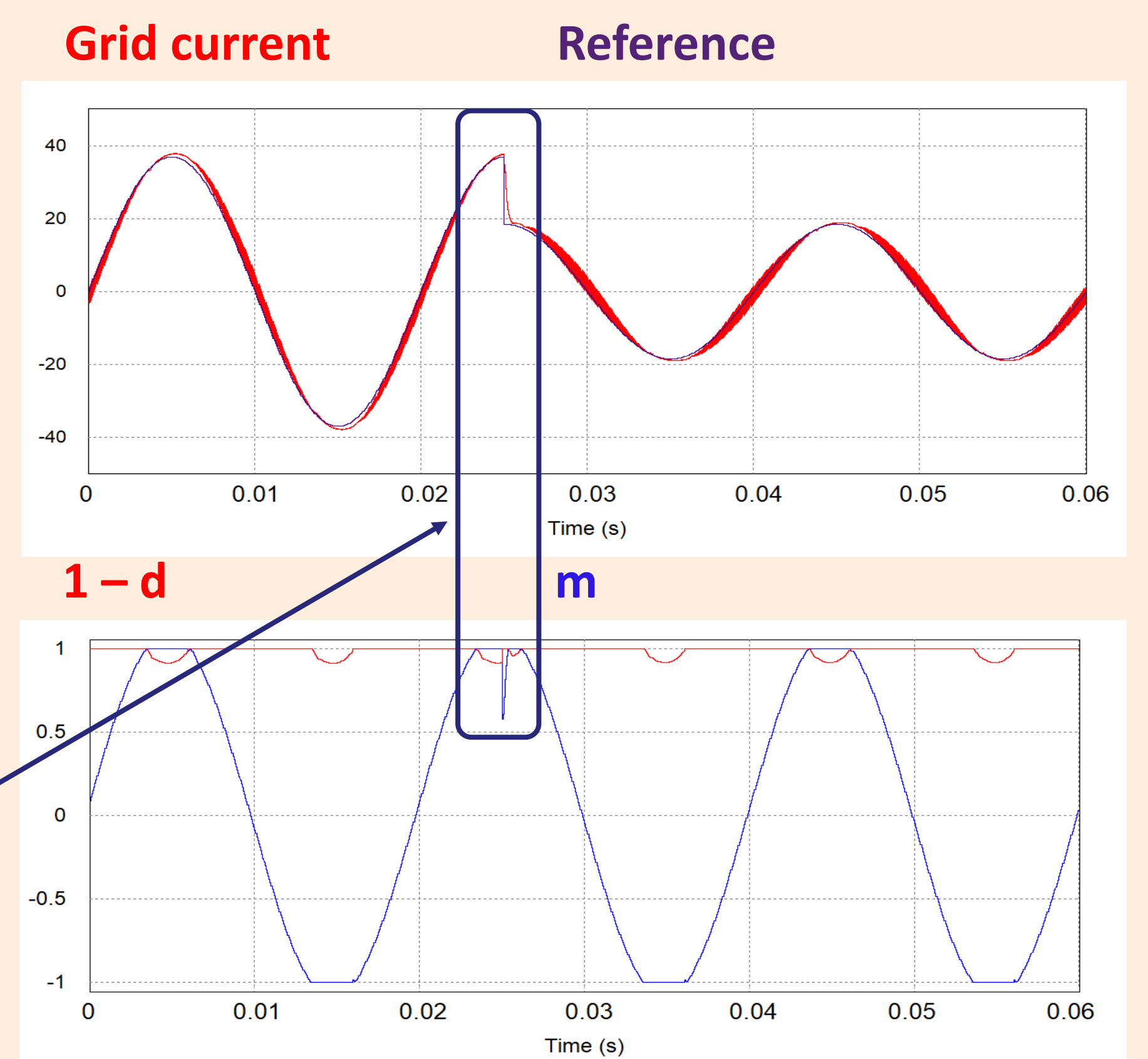
Soft-transition between Buck mode and Boost mode

PV generator at MPP

$$v_{in} = 263 \text{ V}$$

$$THD = 2.82\%$$

Current control loop dynamic response: step from nominal power output to 50% power output.



CONCLUSION

- By applying the proposed feed-forward compensations only one controller is used for both operating modes.
- The proposed dual-mode control method achieves high-quality grid current and fast dynamic response, as shown by the simulation results.