

1 the root mean square method (I_{RMS}). Many parameters had high degrees of correlation
2 with each other, and therefore gave almost identical information. The results of this study
3 may contribute to the understanding of the surface roughness phenomenon and its
4 parameterisation in agricultural soils.

5 **Keywords:** surface roughness, roughness parameters, agricultural soils, tillage

6

7 **1. Introduction**

8 Surface roughness is a key element in the hydrological and erosive behaviour of soils
9 (Helming et al., 1998), and as a soil-atmosphere frontier, plays an important role in many
10 processes, such as infiltration, runoff, the detachment of soil due to water or wind, gas
11 exchange, evaporation and heat fluxes (Huang and Bradford, 1992).

12 Depending on the order of magnitude of the soil surface elevation variations, and on the
13 spatial arrangement of its microforms, surface roughness can be classified into different
14 categories (Römken and Wang, 1986): (1) Variations in the soil's microrelief due to its
15 individual particles and/or microaggregates (variations of the order of 1 mm, but up to 2
16 mm). (2) Variations in the surface generated by soil clods caused by agricultural practices
17 (variations of the order of 100 mm, but up to 200 mm); these two roughness types are
18 considered random and isotropic (i.e., uniform in all directions). (3) Roughness due to the
19 systematic differences in elevation (i.e., rows or furrows) caused by tillage implements
20 (variations between 100-200 mm); these forms are one-directional and this component is,
21 therefore, oriented or anisotropic. (4) Roughness due to the macroforms of the terrain (of
22 the order of several meters), which together define the topography of the landscape; these
23 elevation variations are usually non-directional. Although the classification of Römken
24 and Wang (1986) associated the effect of tillage with an oriented type of roughness

1 (category 3), it is understood that random roughness (categories 1 and 2) is also affected,
2 to a greater or lesser extent, by tillage.

3 The order of magnitude in the elevation variations of the two (or three) first roughness
4 types is lower than the spatial resolution of the digital elevation models that are
5 conventionally used (Govers et al., 2000; Mushkin and Gillespie, 2005). Hence, in order
6 to quantitatively characterise those microforms, it is necessary to take complementary
7 measurements *in situ*, which permit the calculation of different surface roughness
8 parameters or indices.

9 The parameterisation of the random surface roughness caused by tillage (the first two
10 categories cited above) is not straightforward. Each tillage practices (or implements)
11 causes, in theory, a particular type of microrelief under identical soil conditions (in terms
12 of texture, moisture, density, etc.). Considering the wide range of possible soil conditions,
13 a huge variety of roughness types could be found in agricultural soils immediately after
14 tilling. In addition, soil physical properties, particularly surface roughness, can also be
15 highly variable in space. To further complicate its characterisation, surface roughness also
16 shows a multi-scale nature making any roughness measurement scale-dependent
17 (Zhixiong et al., 2005; Verhoest et al., 2008; Álvarez-Mozos et al., 2011). Finally, the
18 microrelief generated by the different tillage practices is more or less susceptible to
19 change throughout time due to the action of meteorological agents, e.g., precipitation
20 (Dalla Rosa et al., 2012), wind and temperature changes in the low atmosphere (Pardini,
21 2003), or even animal activity.

22 Although there are many parameters and indices for quantifying surface roughness (e.g.,
23 Helming et al., 1993; Magunda et al., 1997; Kamphorst et al., 2000; Vermang et al.,
24 2013), none work universally and interested scientists/technicians find it difficult to select
25 the most appropriate one for their particular case. The random roughness parameters that

1 are most commonly used in the literature, described in section 2.3, were considered in
2 this study; these parameters can be divided into four groups, following a criterion similar
3 to that of Smith (2014): (1) parameters measuring the vertical dimension of roughness or
4 the magnitude of the elevation variations of the points at the soil surface (vertical
5 parameters), (2) parameters measuring the horizontal dimension of roughness or the
6 relation between the height of a point and that of its neighbours (horizontal parameters),
7 (3) parameters combining both dimensions (combined parameters), and (4) parameters
8 based on fractal theory, which measure self-affinity or the balance between height
9 variations at different spatial scales (fractal parameters).

10 In light of the above, the aim of this research was to evaluate and select the most
11 appropriate surface roughness parameters to characterise and quantify the surface
12 roughness caused by typical tillage operations.

13

14 **2. Material and methods**

15 *2.1. Test site*

16 Roughness data were taken in 10 agricultural fields, with an extension ranging from 3 ha
17 to 7.3 ha. Fields were located in the experimental hydrological watershed of La Tejería
18 (N42°44'10.6'' and W1°56'57.2'') in Navarre (Spain), which has been used in different
19 research works in the past (e.g., Casalí et al., 2008; Álvarez-Mozos et al., 2009; Álvarez-
20 Mozos et al., 2011). Each of the fields was subjected to different tillage operations (see
21 Fig. 1.A-E and Table 1) following the conventional soil preparation calendar in the area.
22 Thus, during the months of September and October, 2004, the obtained data corresponded
23 to soils subjected to primary tillage, i.e., classes Mouldboard Plough (MP), Harrowed
24 Rough (HR), and Harrowed Smooth (HS). In the month of November 2004, soils were

1 sown with cereal crops, representing typical seedbed conditions; this class was referred
2 to as Planted Unmodified (PU). Finally, a final measurement was carried out in March
3 2005. By this time, seedbed soils had been modified by the action of the rainfall that had
4 occurred since sowing (~250 mm); this class was referred to as Planted Modified (PM).
5 In total, 164 profiles were taken (see Table 1). Profiles were measured in parallel to tillage
6 rows, to reflect the random roughness component.

7 Insert Figure 1 here

8 Insert Table 1 here

9 2.2. Profile measurements

10 Profiles were taken with a profilometer designed *ad hoc* for roughness measurement
11 (Álvarez-Mozos et al., 2005). This instrument incorporates a laser sensor that measures
12 the vertical distance from a reference bar down to the surface. The laser profilometer (see
13 Fig. 1.F) consists of an aluminium bar with its ends fixed to two tripods. The laser distance
14 meter is located inside a case that moves along the aluminium bar, propelled by a small
15 electric motor. The laser profilometer has a vertical accuracy of 1.25 mm and a
16 measurement interval of 5 mm. The total length of profiles was 5 m, so that in each one
17 there are 1000 height records.

18 Profiles were processed using a code developed *ad hoc*, consisting of: (1) the correction
19 of the buckling effect on the aluminium bar by detrending profiles with a parabolic curve
20 obtained from a perfect horizontal reference surface, (2) the application of a filter to
21 eliminate the outliers eventually detected in the height records (e.g., plant material) by
22 deleting and interpolating records with height differences larger than 10 cm with the
23 previous and next records, and (3) the correction of terrain slope (i.e., profile detrending)
24 through the subtraction of the linear trend observed in the data (Xingming et al., 2014).

1 Once this process had been carried out, the profiles were ready for the calculation of the
2 different roughness parameters.

3 It should be noticed that the data analysed in this study are 2D profiles and that inferences
4 about 3D phenomena (e.g., depression storage) should be made with caution.

5 *2.3. Calculation of roughness parameters*

6 In total, 21 surface roughness parameters were analysed (Table 2); these parameters could
7 be classified into vertical, horizontal, combined, and fractal parameters, as explained in
8 the introduction. Next, each parameter is briefly described; parameter names are
9 highlighted in bold for clarity.

10 Insert Table 2 here

11 Random roughness, one of the indices most frequently used to describe surface
12 roughness, was proposed by Allmaras et al. (1966) as the standard deviation of heights
13 after the elevations were transformed to natural logarithms and corrected for slope and
14 tillage tool marks. After Currence and Lovely (1970) showed that the parameter was more
15 sensitive without any logarithmic transformation, most authors (e.g., Bertuzzi et al., 1990;
16 Hansen et al., 1999; Kamphorst et al., 2000) calculate random roughness as the **standard**
17 **deviation of heights** (s) (eq. 1):

$$18 \quad s = \sqrt{\frac{\sum_{i=1}^N (z_i^2 - \bar{z}^2)}{N-1}} \quad (1)$$

19 where N is the number of height records, z_i is the height corresponding to record i , and \bar{z}
20 is the mean height of all the records.

21 The **correlation length** (l_{ACF}) represents the horizontal component of roughness, i.e., it
22 describes the relative location of heights or the way in which the heights vary along the

1 surface (Ogilvy and Foster, 1989). The correlation length was calculated from the
 2 autocorrelation function (eq. 2) (Ulaby et al., 1982):

$$3 \quad \rho(h) = \frac{\sum_{i=1}^{N(h)} z_i z_{i+h}}{\sum_{i=1}^N z_i^2} \quad (2)$$

4 where $\rho(h)$ is the autocorrelation function, which represents the correlation existing
 5 between height z of the point i (z_i) and that of another point located at a lag distance h
 6 from it (z_{i+h}), and $N(h)$ is the number of pairs considered in each lag h . The correlation
 7 length (l_{ACF}) is then defined arbitrarily as the distance at which the heights of two points
 8 on the surface are considered independent; i.e., $\rho(h)$ is equal to $1/e$, so that $\rho(l) = 1/e$.
 9 Another parameter extracted from the autocorrelation function is its **initial slope** ($\rho'(0)$),
 10 which also provides a measure of the horizontal roughness (Borgeaud et al., 1995), but in
 11 this case at a more local scale, i.e., focusing on the height variations of a point with its
 12 nearest neighbours. Zribi and Dechambre (2003) proposed **parameter** Z_s as a
 13 combination of s and l_{ACF} (eq. 3), and thus accounted for both vertical and horizontal
 14 roughness components:

$$15 \quad Z_s = s^2 / l_{ACF} \quad (3)$$

16 The concepts of the **limiting elevation difference** (LD) and the **limiting slope** (LS) were
 17 developed to include the spatial aspect of roughness (Linden and Van Doren, 1986).
 18 Parameter LD supplies information on the characteristics of roughness at long distances,
 19 whereas LS is used to characterise roughness at short distances (Bertuzzi et al., 1990).
 20 The mean absolute-elevation-difference is defined as (eq. 4):

$$21 \quad \Delta z_h = \sum_{i=1}^{N(h)} \frac{|z_i - z_{i+h}|}{N(h)} \quad (4)$$

22 The relationship between Δz_h and the lag distance h was obtained from a hyperbolic
 23 linear model defined by (eq. 5):

1 $1/\Delta z_h = a + b(1/h)$ (5)

2 where a and b are the fitting parameters obtained for an arbitrary horizontal distance.
 3 After testing different values, and following the recommendation of Linden and Van
 4 Doren (1986), this distance was set to 20 cm. Parameter LD (eq. 6) determines the shape
 5 of the variogram, assumed to follow a hyperbolic function:

6 $LD = 1/a$ (6)

7 Parameter LS (eq. 7) is the original variogram slope (Kamphorst et al. 2000), given by:

8 $LS = 1/b$ (7)

9 Linden et al. (1988) proposed a third parameter that was obtained as a combination of
 10 parameters LD and LS , called **parameter Q** (eq. 8). This parameter can be considered a
 11 combined roughness parameter.

12 $Q = (LD \cdot LS)^{1/2}$ (8)

13 The semivariogram represents how height data are related to distance. The semivariance
 14 function depending on the lag h can be calculated as:

15 $\gamma(h) = \frac{1}{2N(h)} \sum_{i=1}^{N(h)} [z_{i+h} - z_i]^2$ (9)

16 Once the experimental semivariogram was calculated, a spherical model was fitted to it
 17 (Vázquez et al., 2009; Croft et al., 2013):

18 $\gamma(h) = \begin{cases} c_1 \left[1.5 \frac{h}{h_a} - 0.5 \left(\frac{h}{h_a} \right)^3 \right] + c_0 ; h \leq h_a \\ c_1 + c_0 ; h > h_a \end{cases}$ (10)

19 where h_a is the Range, c_1 is the Sill, and c_0 is the Nugget. After testing different values,
 20 100 cm of maximum lag distance was deemed sufficient to accurately fit the spherical
 21 model to the experimental semivariogram. **Sill** represents the value of $\gamma(h)$ where the

1 fitted model reaches the plateau, and **Range** is the distance at which the *Sill* is found. No
 2 nugget effect was taken into account (Vermang et al., 2013). Both *Sill* and *Range* have
 3 been frequently used as soil surface roughness indices (e.g., Helming et al., 1993;
 4 Vázquez et al., 2009; Croft et al., 2009, Croft et al., 2013; Vermang et al., 2013).

5 **Parameter MIF** (eq. 11) was formulated by Römken and Wang (1986) with the aim of
 6 quantitatively describing surface roughness. This dimensionless parameter represents the
 7 integrated effect of the **peak frequency** (F) and the **microrelief index** (MI), and it is
 8 defined arbitrarily as:

$$9 \quad MIF = MI \cdot F \quad (11)$$

10 where MI represents the area per unit of length between the measured surface profile and
 11 the regression line of least squares through all measured elevations on a transect
 12 (Römken and Wang, 1986), and F is the number of peaks (i.e., points with higher
 13 elevations than their neighbours on both sides) per unit of length of the profile. Parameters
 14 MI and F (eq. 11) are evaluated separately as descriptive parameters of vertical and
 15 horizontal roughness, respectively.

16 The **Mean Upslope Depression index** (MUD) (eq. 12) was specifically developed to
 17 predict surface storage capacity (Hansen et al., 1999). The MUD is based on the elevation
 18 differences ($z_i - z_{i+h}$) between a reference point i and another $i+h$ on a line segment
 19 positioned upslope from the reference point. Within each line segment, the calculation
 20 procedure is iterated for a number of sub-segments, each time taking a new upslope point
 21 as the reference point (Hansen et al., 1999):

$$22 \quad MUD = \sum_{i=1}^m \left(\sum_{j=1}^n \frac{\Delta z}{n} \right) / m \begin{cases} \Delta z = z_i - z_{i+h} ; z_i \geq z_{i+h} \\ \Delta z = 0 ; z_i < z_{i+h} \end{cases} \quad (12)$$

1 where n is the number of points in a line sub-segment and m is the number of line sub-
2 segments. In Hansen et al. (1999), no particular segment length was recommended, but
3 they considered a 30-cm length for their conditions. In our case, after testing different
4 values, a segment length of 20 cm was selected.

5 **Tortuosity** is a roughness index based on the ratio of the surface profile perimeter length
6 (L_1) and its horizontal projection (L_0). Although variants do exist (e.g., Boiffin, 1984;
7 Planchon et al., 1998), the present study used the tortuosity index of Saleh (T_S) (eq. 13)
8 (Saleh et al., 1993):

$$9 \quad T_S = 100 \cdot \frac{(L_1 - L_0)}{L_1} \quad (13)$$

10 Different methods have been used to calculate the **fractal dimension** (and in some cases
11 the **crossover length**), which characterises the self-affinity of surface roughness profiles.
12 The **semivariogram method** (SMV) was introduced to study the variability of soil
13 properties and subsequently used to quantify roughness (Burrough, 1983a,b; Armstrong,
14 1986; Huang and Bradford, 1992; Vidal Vázquez et al., 2005; Chi et al., 2012; Vermang
15 et al., 2013). The first step in the estimation of the fractal dimension is the calculation of
16 the experimental semivariogram (eq. 9) (Vidal Vázquez et al., 2005). Assuming a fractal
17 Brownian motion (fBm) model, the experimental semivariogram can be described as a
18 function of the lag (Eq. 14):

$$19 \quad \gamma(h) = l^{1-H} h^H \quad (14)$$

20 where l is the crossover length and H is the Hurst coefficient. After a log-log
21 transformation of eq. 14, H can be estimated as the slope of the semivariance versus the
22 lag distance. When applied to surface roughness profiles, the logarithmic transformation
23 normally yields a curved trend rather than a line, thus revealing a multi-fractal nature
24 (Vidal Vázquez et al., 2005; Moreno et al., 2008). In this study, only the fractality of the

1 first stretch (where the linear assumption holds) was measured. For that purpose, a
 2 maximum lag distance of 10 cm was considered because it provided a good fit to the
 3 linear trend in all the profiles. Afterward, the Hurst coefficient was related to the fractal
 4 dimension as follows (Smith, 2014) (eq. 15):

$$5 \quad D_{SMV} = 1 + d - H = 2 - H \quad (15)$$

6 where d is the Euclidean dimension of the system (i.e., 1 for profiles, 2 for surfaces, etc.).
 7 Further, the crossover length (l_{SMV}) (eq. 16) can be calculated as follows (Huang and
 8 Bradford, 1992):

$$9 \quad l_{SMV} = \exp \left[\frac{a_{SMV}}{(2-2H)} \right] \quad (16)$$

10 where a_{SMV} is the intercept of the linear trend fitted to the first stretch of the
 11 semivariogram.

12 The **root mean square method** (RMS) is based on the evaluation of the root mean square
 13 deviation of elevation values for increasing lag distances, and it has been used in different
 14 studies (Malinverno, 1990; Gallant et al., 1994; Moreira et al., 1994; Vidal Vázquez et
 15 al., 2005). The average RMS values for increasing lag distances (h) are calculated as
 16 (Vidal Vázquez et al., 2005):

$$17 \quad \bar{W}(h) = \frac{1}{n_h} \sum_{u=1}^{n_h} \left\{ \frac{1}{n} \sum_{i \in h} [z_i - \bar{z}_h]^2 \right\}^{1/2} \quad (17)$$

18 where n_h is the total number of lags of size h and \bar{z}_h represents the average elevation
 19 values for all points of each lag. As in the semivariogram method, the slope of the
 20 logarithmic transformation of $\bar{W}(h)$ gives an estimation of the Hurst coefficient, which
 21 enables the calculation of the fractal dimension (D_{RMS}) and the crossover length (l_{RMS})
 22 (eq. 15 and 16).

1 The estimation of the fractal dimension by the **box counting method** (BC) is motivated
2 by the scale law defined by Mandelbrot (1977):

$$3 \quad D(r) = \frac{\log(N_r)}{\log(1/r)} \quad (18)$$

4 where N_r stands for the minimum number of boxes of a width r that can cover the object
5 (i.e., surface profile). The basic idea is simple since the profile to be studied is initially
6 covered by a single box. That box is divided into 4 quadrants, and the number of quadrants
7 required to cover the profile are counted. Then, each quadrant is divided into another four
8 sub-quadrants, and this division goes on until the width of the boxes reaches the resolution
9 of the data, counting the number of cells required to cover the profile in each step
10 (Gneiting et al., 2012). Function $D(r)$ is transformed into logarithms and fitted to a
11 regression line, from whose slope (α) the fractal dimension D_{BC} (eq. 19) (Liang et al.,
12 2012) is obtained:

$$13 \quad D_{BC} = -\alpha \quad (19)$$

14 A further technique used to determine the Hurst coefficient, and hence the fractal
15 dimension, is the **power spectrum method** (PS) (Gneiting et al., 2012). This estimator is
16 based on the spectral density function $S(\nu)$ for a stationary stochastic process, obtained
17 by the fast Fourier transform (FFT), which depicts how the roughness is distributed in
18 components of different frequencies (ν). The Hurst coefficient is obtained through the
19 regression line of the logarithmic transformation of function $S(\nu)$, and thereafter the
20 fractal dimension (D_{PS}) (eq. 15).

21 Finally, the **rescaled range method** (RS) (Liu and Molz, 1996; Liang et. al, 2012) was
22 also used, which is based on calculating the fitted range R in terms of the lag distance h :

$$23 \quad R(h) = R_a/s(h) \quad (20)$$

1 where R_a is the sum of the absolute values of the largest positive and negative deviations
2 of lag points from its trend line, and $s(h)$ is the standard deviation of each lag. As in the
3 previous cases, to obtain the Hurst coefficient, a linear regression of the logarithmic
4 transformation of $R(h)$ is made, from which the fractal dimension (D_{RS}) (eq. 15) is
5 obtained.

6 *2.4. Parameter evaluation*

7 *2.4.1. Descriptive analysis*

8 To assess the different parameters, first, the different roughness classes were visually
9 analysed. The box plots generated by each of the parameters per roughness class were
10 also visually analysed.

11 *2.4.2. Separability analysis*

12 The evaluated roughness parameters did not necessarily follow Gaussian probability
13 distribution functions, since they might have asymmetric distributions. Furthermore, the
14 different roughness classes did not necessarily have comparable variances. Hence, the
15 comparison of parameters and classes could not rely on classic statistical tools, such as
16 the analysis of variance (requiring Normality and homoscedasticity), and thus the
17 separability analysis was used to select the most suitable parameters for the
18 characterisation of different roughness classes. Separability, or dissimilarity, is a
19 statistical metric that quantifies how different two sets of data are; it can be evaluated by
20 computing different statistical distance measures (e.g., Divergence, Bhattacharyya
21 distance, etc.). In this study, the Jeffries-Matusita Distance (D_{JM}) (Swain and King, 1973)
22 was used, which was calculated for each parameter and pair of roughness classes. D_{JM}
23 (eq. 21) has been frequently used to analyse similarity and feature selection processes,

1 and a good number of studies recommend its use (e.g., Bruzzone et al., 1995; D’Urso and
2 Menenti, 1996):

$$3 \quad D_{JM} = \int \left[\left(\sqrt{f(x)} - \sqrt{g(x)} \right)^2 \right] dx \quad (21)$$

4 where D_{JM} is the distance between classes $f(x)$ and $g(x)$ measured by the parameter x .

5 D_{JM} has a range of variability between 0 and 2, i.e., 0 means $f(x)$ and $g(x)$ completely
6 overlap and 2 means they are completely separable. Values below 1 can be considered of
7 poor separability, whereas values from 1-1.5 corresponds to moderate separability, and
8 1.5-2 to high separability (Skriver, 2007). By using this analysis, we aimed to quantify
9 the ability of the different parameters to discriminate between different roughness classes.

10 *2.4.3. Correlation analysis*

11 A correlation analysis was performed to study the relationships between the different
12 roughness parameters. For this purpose, the Spearman correlation coefficient (R) was
13 calculated, which is particularly indicated for detecting any type of monotonic
14 relationship.

15

16 **3. Results**

17 *3.1. Descriptive analysis*

18 Roughness class MP presented a higher range of variation in its profile elevations (i.e.,
19 vertical roughness) as a result of the presence of soil clods of up to 10 cm in size, with no
20 clear spatial pattern or arrangement (Fig. 2). Visually, classes HR and HS did not exhibit
21 such a large vertical roughness (which was smaller in HS than in HR), but their horizontal
22 roughness seemed greater than in MP, i.e., displaying more serrated profiles. Classes PU
23 and PM showed an even smaller range of vertical variation, and although PU had a high

1 horizontal roughness, the smoothing effect of the rain, which translated into a lesser
2 horizontal roughness, could be clearly seen in PM. In this first visual analysis, they could
3 be ranked –as we understand– in an increasing order of roughness, as follows:
4 $PM < PU < HS < HR < MP$.

5 

6 *3.2. Parameters per roughness class*

7 The behaviour of the different parameters in terms of the roughness classes were analysed
8 using boxplots (Fig. 3). In the vertical parameters the mean class values increased with
9 the roughness, which could be visually observed (Fig. 2). Furthermore, the variability of
10 each class increased as its roughness did, with a minimum variability for classes PM and
11 PU, followed by HS and HR, and with a maximum variability for MP. All in all, different
12 types of tillage (i.e., classes PU, HS, HR, and MP) could be differentiated with relative
13 clarity. The effect of rainfall lowered class PM's values, compared to PU, in most vertical
14 parameters, but their differences were rather small and both classes overlapped to a
15 certain degree.

16 

17 Horizontal parameters did not exhibit the same trend as the vertical ones (Fig. 3).
18 Regarding the variability per class, different patterns were observed for the different
19 parameters, although MP was less variable than the other classes in all parameters.
20 Parameters *LACF* and *Range* behaved similarly, with comparable values for the different
21 classes and many outliers especially in the least rough classes (i.e., PM and PU).
22 Parameters $\rho'(0)$ and *F* followed a similar trend, showing a moderate differentiation
23 between classes PU, HS, HR, and MP; however, the action of precipitation modified that
24 trend and made class PM take lower $\rho'(0)$ and *F* values than PU, indicating a higher

1 correlation between the surface elevations. Finally, parameter LS took increasing values
2 for increasing roughness conditions (i.e., PU, HS, HR, and MP), but there was a high
3 overlap between classes; nevertheless, this parameter seemed to clearly differentiate PM
4 from the other classes.

5 The combined parameters followed a trend similar to the vertical parameters (Fig. 3), i.e.,
6 their values increased with increasing roughness, but the combine parameters did not have
7 the same marked difference in parameter variability than the vertical parameters did, at
8 least not in all cases (see parameters Q and T_s in Fig. 3). Parameters MIF and MUD , and
9 to a lesser extent Z_s , did behave very similarly to the vertical ones, with increases in
10 variability as roughness increased; however, parameter Q did not follow this behaviour,
11 as it had a very similar variability in all the classes. Finally, parameter T_s followed a
12 completely different pattern, with a good separation between classes PM and PU but
13 minor differences between the rest.

14 Regarding fractal parameters, the D values calculated with different techniques behaved
15 similarly, although their absolute values differed slightly (Fig. 3); their performance
16 resembled that of parameter $\rho'(0)$. This pattern indicates a more self-affine behaviour as
17 tillage classes increased in roughness, although the precipitation effect modified that
18 tendency. The variability of the fractal dimensions was rather homogeneous for all the
19 classes, but the crossover lengths behaved completely differently. Parameter l_{SMV}
20 followed a very similar trend to the mixed parameters Q and MUD , with incrementing
21 values for roughness classes, and a very homogeneous variability for all of them.
22 Meanwhile, parameter l_{RMS} was similar to the horizontal parameter LS , with similar values
23 for most tillage classes, but with a clear differentiation of class PM.

24 3.3. Separability between roughness classes

1 The vertical parameters and the combined parameters MUD and Q showed better mean
2 separability with D_{JM} values >1 (Table 3). More precisely, parameters LD and MUD were
3 those with a higher mean separability ($D_{JM} \sim 1.25$). The rest of the combined parameters
4 (MIF , Z_S and T_S) offered moderate separabilities ($D_{JM} \sim 0.9$). The horizontal parameters
5 displayed somewhat lower mean separabilities, with D_{JM} values of 0.6-0.7, but in the case
6 of l_{ACF} and $Range$, D_{JM} did not reach 0.3. Lastly, the fractal dimensions calculated with
7 different techniques followed similar patterns, although their mean separabilities varied
8 significantly, from 0.92 (D_{RMS}) to 0.52 (D_{RS}), though the crossover lengths behaved
9 differently. Parameter l_{SMV} ended up reaching a higher separability than 1, while
10 parameter l_{RMS} hardly exceeded the mean separability of 0.4.

11 Insert Table 3 here

12 The vertical parameters had the highest separability values between classes PU, HS, HR,
13 and MP, especially parameter LD , but none of the vertical parameters was particularly
14 successful at detecting rainfall smoothening, i.e., separating PM and PU, since in no case
15 did D_{JM} reach values above 0.4 for these two classes. Separability values between
16 neighbouring tillage classes (i.e., PU vs. HS, HS vs. HR, and HR vs. MP) were not high
17 for any of the vertical parameters; $Sill$ and LD functioned best in these cases. For
18 horizontal parameters, separability between class pairs was generally lower than for
19 vertical parameters. Nevertheless, the highest D_{JM} value between classes PM and PU was
20 obtained by parameter LS with a value ~ 0.9 . The behaviour of the combined parameters,
21 once more, was similar to the vertical ones, offering separabilities comparable to those,
22 especially for parameters MUD and Q . Regarding the separation between classes PM and
23 PU, better separabilities were obtained than with the vertical parameters (especially for
24 T_S , Z_S , and Q), although still lower than those of LS . In addition, parameters Q , MUD , and
25 T_S offered the highest separabilities between PM and classes HS, HR, and MP. Lastly,

1 regarding fractal parameters, although the different dimensions did not generally exhibit
2 high separabilities, D_{RMS} had some of the highest separabilities between PU and classes
3 HR and MP and between HS and HR and MP, and D_{BC} had the highest separability
4 between classes PU and MP. Regarding the crossover lengths, although the separability
5 between the different tillage types (PU, HS, HR, and MP) was not high, the good
6 separability obtained between class PM and the rest was highly noteworthy (especially
7 for l_{SMV}).

8 3.4. Parameter correlation

9 With regard to the correlations between parameters of one type, the vertical parameters
10 were highly correlated with each other, with $R \sim 0.9$ (Fig. 4); however, the horizontal
11 parameters showed more heterogeneous behaviour with different R values. Parameters
12 l_{ACF} and $Range$ had a good correlation ($R \sim 0.85$), as did $\rho'(0)$ with F , l_{ACF} , and $Range$
13 (although slightly lower, $R \sim 0.6$), but the other parameters had relatively low correlations.
14 Parameter LS , in general, had low correlations with the rest of the horizontal parameters.
15 On the other hand, mixed parameters showed quite homogeneous behaviour with high
16 correlations ($R \sim 0.9$) with each other, but a little lower for Z_S and MIF ($R \sim 0.75$). Finally,
17 the different fractal dimensions showed high correlations between each other ($R \geq 0.8$),
18 except for parameter D_{RS} ($R \sim 0.6$). The crossover lengths (l_{SMV} and l_{RMS}) were only
19 moderately correlated ($R \sim 0.6$).

20 Insert Figure 4 here

21 Overall, vertical parameters correlated well with mixed ones ($R \geq 0.8$), except for Z_S and
22 T_S , which had somewhat lower correlations ($R \sim 0.6$). A negative correlation was found
23 between the vertical parameters and fractal dimensions, although they measure different
24 phenomena; this would indicate that the greater the vertical roughness, the more self-

1 affine a surface is. The crossover lengths (l_{SMV} and l_{RMS}) presented a disparate behaviour.
2 Although l_{SMV} had a good correlation with the different fractal dimensions (negative
3 correlation), F (negative correlation), and most vertical and combined parameters, l_{RMS}
4 had no correlations with the different fractal dimensions and lower correlations than l_{SMV}
5 with the vertical and combined parameters. In both cases, the correlation with parameter
6 LS was high, especially in the case of l_{RMS} ($R \geq 0.9$).

7

8 **4. Discussion**

9 *4.1. Differentiation between tillage types*

10 The values of s and LD obtained for the different classes are comparable to those reported
11 in the literature for similar conditions (e.g., Zobeck and Onstad, 1987; Helming et al.,
12 1993; Arvidsson and Bolenius, 2006; Bauer et al., 2015). In the absence of significant
13 changes caused by the rainfall, s and LD have been successfully related to the size of soil
14 clods and then proposed as good indices for distinguishing different tillage types
15 (Helming et al., 1993; Eltz and Norton, 1997; Magunda et al., 1997; Kamphorst et al.,
16 2000; Vermang et al., 2013; Bauer et al., 2015). The values of $Sill$ obtained here were
17 considerably higher (although within the range of variation) than those reported by
18 Helming et al. (1993) and Vermang et al. (2013), partly because their experiments were
19 carried out using artificial roughness and because of the measurement scale.

20 Regarding the horizontal parameters, there is no agreement in the literature. For instance,
21 several authors reported increasing values of l_{ACF} for increasing roughness conditions
22 (Davidson et al., 2003; Baghdadi et al., 2008), while others observed more similar
23 behaviour to that obtained here, with no clear differences between roughness classes
24 (\acute{A} lvarez-Mozos et al., 2005; Verhoest et al., 2008). The *Range* values obtained in this

1 study were, in general, higher (although within the range of variation) than those reported
2 by other authors (Helming et al., 1993; Vermang et al., 2013), but with an important
3 overlap between classes and frequent outliers. Parameters l_{ACF} and $Range$ were obtained
4 using different techniques but represent analogous concepts (Vidal Vázquez et al., 2005),
5 and this is corroborated by the results presented here. Parameters $\rho'(0)$ and F were the
6 horizontal parameters that best differentiated tillage classes; this is due to the geometry
7 of the microforms presented in the smooth classes and the macroforms presented in the
8 roughest classes, since the smaller the size of the clods, the more parameter F increased
9 (Bertuzzi et al., 1990). This same phenomenon explains that the reason that $\rho'(0)$ took
10 lower values in the roughest classes was due to the presence of macroforms, which made
11 the autocorrelation function descend more gently in these classes, whereas it did so more
12 abruptly in smoother tillage classes with greater microform presence.

13 On the other hand, the combined parameters have been rarely used as an approach to
14 separate tillage types. Baghdadi et al. (2008) mentioned that parameter Z_s took on values
15 of <0.1 cm for smooth soils and >0.1 cm for ploughed ones, but did not investigate
16 different tillage practices in greater detail. Zribi and Dechambre (2003) found a direct
17 correlation between the values of Z_s and the clod's size; they reported a variation range
18 of Z_s between 0.07 cm and 1.93 cm for agricultural soils. This trend agrees with our
19 results, although we observed considerable overlapping between similar tillage classes
20 and a slightly narrower range of values. On the other hand, MIF appeared to be good
21 parameter to separate different tillage classes (Lehrsch et al., 1988; Bertuzzi et al., 1990).

22 In fractal parameters, although some authors found that the values of fractal dimensions
23 and their respective crossover lengths (calculated with different techniques) should be
24 relatively similar (Vidal Vázquez et al., 2005; Vivas Miranda et al., 2002), there is not
25 always an agreement between the values shown in different works. For instance, some

1 authors (e.g., Gallant et al., 1994) found substantial variations between methods. In our
2 case, despite the differences in magnitude, we observed that the behaviour was very
3 similar in the different procedures used. This is in accord (except for the case of l_{RMS})
4 with Chi et al. (2012), who concluded that, generally, the fractal dimension (parameter
5 D) decreased and the crossover length (parameter l) increased with the increment of soil
6 clods. Vermang et al. (2013) also reported that the rougher the surface, the lower
7 parameter D was.

8 For all the above, parameter LD is recommended to separate the different types of tillage
9 studied in terms of the vertical roughness, parameter $\rho'(0)$ in terms of the horizontal
10 roughness, parameter MUD in terms of both properties, and parameter D_{RMS} in terms of
11 its self-affinity.

12 *4.2. Effect of rainfall on the different roughness parameters*

13 Although the values of all the vertical parameters changed after successive rainfalls, those
14 changes were not significant enough to clearly differentiate the precipitation effect
15 (Huang and Bradford, 1992; Vermang et al., 2013). In this sense, Bertuzzi et al. (1990)
16 and Magunda et al. (1997) found that parameters representing the roughness' vertical
17 component were good indicators of roughness at higher scales (and then useful to
18 differentiate tillage types), whereas the horizontal parameters were appropriate at lower
19 scales (and hence suitable to evaluate changes in roughness due to rainfall).

20 As opposed to the vertical parameters, in Vermang et al. (2013), the values of $Range$ and
21 l_{ACF} increased after rainfall events (applied with a rain simulator). Helming et al. (1993)
22 and Croft et al. (2009) also observed an increase in parameter $Range$ after rain, which
23 Helming et al. (1993) attributed to the smoothing and broadening of the largest soil clods,
24 and Croft et al. (2009) indicated a higher spatial correlation. From a semivariogram

1 analysis, Helming et al. (1993) and Vermang et al. (2013) observed that, on surfaces with
2 small roughness, rain events gave rise to more erratic *Range* patterns. Our results are in
3 agreement with these trends, since the rainfall led to a reduction in vertical parameter
4 values and increases in the *Range* and l_{ACF} values.

5 There were other parameters that displayed a greater sensitivity to the effect of rain.
6 Parameter *LS* was the most sensitive to the changes in roughness caused by precipitation,
7 followed by l_{RMS} and l_{SMV} or T_S . Taconet and Ciarletti (2007) concluded that T_S was a
8 more suitable parameter than s to detect soil smoothing due to rain. With regard to the
9 fractal dimensions, in contrast to what was observed here, Vermang et al. (2013) reported
10 that parameter D increased after rain events in the soils with small roughness, while it
11 decreased in very rough soils. Eltz and Norton (1997) also observed an increase in
12 parameter D and a reduction in l after precipitation. Further, Vidal Vázquez et al. (2007)
13 and Paz-Ferreiro (2008) found similar behaviour to that seen here, with reductions both
14 in D and in l after rain.

15 Some of these variations can be, to some extent, explained if we take into account that
16 rain can either smoothen the roughness, if the sealing processes in the soil are dominant,
17 or increase roughness, if rills or gullies are developed (Vermang et al., 2013). The soils
18 studied here had a single tillage treatment modified by the precipitation (roughness class
19 PM), so that in order to confirm these trends, it would be necessary to carry out similar
20 experiments in all the other treatments.

21 *4.3. Correlation between parameters*

22 Most of our findings are in agreement with previous investigations. We observed a strong
23 correlations between the vertical parameters, such as: s and LD (Linden and Van Doren,
24 1986; Bertuzzi et al., 1990; Magunda et al., 1997); s and $Sill$ (Croft et al., 2013); LS and

1 T_S (Bertuzzi et al., 1990); l_{ACF} and $Range$ (Vidal Vázquez et al., 2005); and s and D_{SMV}
2 (negative correlation) (Chi et al., 2012). However, some of our results partly disagreed
3 with previous findings, e.g., the lack of correlation between MIF and other parameters,
4 such as s or T_S (Bertuzzi et al., 1990), or the high correlation between s and LS (Magunda
5 et al., 1997).

6

7 **5. Conclusions**

8 In this study, the most widely used roughness parameters in earth sciences were selected
9 and their ability to discriminate between the different soil roughness classes created by
10 typical tillage operations was evaluated.

11 Vertical and combined parameters took higher values as tillage became rougher.
12 Horizontal parameters did not show such a clear pattern, with some parameters being
13 rather insensitive to tillage (l_{ACF} and $Range$), and other increasing (LS) and some others
14 decreasing ($\rho'(0)$ and F) as tillage became rougher. On the contrary, the different fractal
15 dimensions that were tested showed a consistent behaviour, with values decreasing (more
16 auto-affine behaviour) as tillage became rougher. All in all, the best parameters for
17 differentiating and characterising different tillage types were LD and MUD .

18 The effect of rainfall was apparent in most parameters. The ones most sensitive to rainfall
19 action were the horizontal parameter LS , the crossover lengths (l_{SMV} and l_{RMS}), and, to a
20 lesser extent, the combined parameter T_S .

21 Many of the evaluated parameters were highly correlated with each other (all the vertical
22 parameters or the combined parameters Q and MUD) and therefore provided almost
23 identical information. For these, our recommendation is to select the simplest ones (i.e.,
24 s or MUD); however, some parameters showed low correlation values with the rest, since

1 they offered complementary information (i.e., I_{SMV} , LS , or I_{ACF}). These parameters could
2 be interesting depending on the particular application pursued.

3 It is expected that the results of this study could contribute to the understanding of the
4 surface roughness phenomenon and to its parameterisation in agricultural soils; however,
5 more research is needed to better characterise roughness dynamics due to the action of
6 rainfall.

7

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12

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1 Table 1. Description of the different roughness classes triggered by agricultural
 2 treatments.

Tillage class	Acronym	Profiles	Description
Mouldboard Plough	MP	20	Tillage operation performed with a plough with multiple mouldboards at a depth of 15-20 cm, resulting in soil inversion and a very rough surface
Harrowed Rough	HR	43	Operation performed normally with a tine harrow to break soil clods and provide a smoother surface suitable for seeding
Harrowed Smooth	HS	29	In cases where the first harrowing did not smoothen sufficiently the surface a second harrowing is applied
Planted Unmodified	PU	44	Seeding operation performed with conventional sowing machinery, normally seed drills
Planted Modified	PM	28	Planted soils modified by the action of the precipitation during 4 months (~250 mm)

3

4

1 Table 2. Summary of roughness parameters analysed.

Type	Parameter	Description	Reference
Vertical	s (cm)	Standard deviation of the heights	Allmaras et al., 1966
	LD (cm)	Limiting elevation difference	Linden and Van Doren, 1986
	$Sill$ (cm ²)	Sill of the semivariogram	Croft et al., 2013
	MI (cm)	Microrelief index	Römken and Wang, 1986
Horizontal	l_{ACF} (cm)	Correlation length	Ulaby et al., 1982
	$\rho'(0)$	Initial slope of the auto-correlation function	Ulaby et al., 1982
	LS	Limiting slope	Linden and Van Doren, 1986
	$Range$ (cm)	Range of the semivariogram	Croft et al., 2013
	F (cm ⁻¹)	Peak frequency	Römken and Wang, 1986
Combined	Z_S (cm)	Combined parameter	Zribi and Dechambre, 2003
	Q (cm ^{1/2})	Combined parameter	Linden et al., 1988
	MIF	Combined parameter	Römken and Wang, 1986
	MUD (cm)	Mean Upslope Depression index	Hansen et al., 1999
	T_S	Tortuosity	Saleh et al., 1993
Fractals	D_{SMV}	Fractal dimension (“semivariogram” method)	Vidal Vázquez et al., 2005
	D_{RMS}	Fractal dimension (“root mean square” method)	Vidal Vázquez et al., 2005
	D_{BC}	Fractal dimension (“box counting” method)	Gneiting et al., 2012
	D_{PS}	Fractal dimension (“power spectrum” method)	Gneiting et al., 2012
	D_{RS}	Fractal dimension (“rescaled range” method)	Liu and Molz, 1996
	l_{SMV} (cm)	Crossover length (“semivariogram” method)	Vidal Vázquez et al., 2005
	l_{RMS} (cm)	Crossover length (“root mean square” method)	Vidal Vázquez et al., 2005

2

3

1 Table 3. Separability (D_{JM}) of the parameters per pairs of roughness classes. The
 2 parameter with the highest separability is in dark grey, and the other two parameters with
 3 a high separability for each pair of classes in pale grey.

Parameter	Separability between classes										Mean
	PM-PU	PM-HS	PM-HR	PM-MP	PU-HS	PU-HR	PU-MP	HS-HR	HS-MP	HR-MP	
<i>s</i> (cm)	0.23	1.03	1.61	1.84	0.64	1.33	1.75	0.28	1.24	0.80	1.07
<i>LD</i> (cm)	0.40	1.61	1.67	1.92	0.72	1.25	1.81	0.73	1.64	0.80	1.26
<i>Sill</i> (cm ²)	0.27	1.07	1.45	1.68	0.73	1.25	1.59	0.27	1.16	0.87	1.03
<i>MI</i> (cm)	0.20	0.99	1.58	1.82	0.60	1.29	1.73	0.27	1.23	0.81	1.05
<i>l_{ACF}</i> (cm)	0.09	0.08	0.17	0.73	0.01	0.02	0.52	0.03	0.58	0.46	0.27
$\rho'(0)_{ACF}$	0.40	0.09	0.11	1.00	0.15	0.82	1.66	0.34	1.11	0.83	0.65
<i>LS</i>	0.90	1.38	1.47	1.70	0.11	0.16	0.29	0.01	0.06	0.04	0.61
<i>Range</i> (cm)	0.05	0.08	0.27	0.17	0.01	0.16	0.13	0.12	0.11	0.08	0.12
<i>F</i> (cm ⁻¹)	0.02	0.43	0.59	1.19	0.58	0.78	1.41	0.28	0.76	0.21	0.62
<i>Z_s</i> (cm)	0.69	1.26	1.44	1.83	0.24	0.71	1.39	0.37	0.98	0.21	0.91
<i>Q</i> (cm ^{1/2})	0.65	1.67	1.75	1.97	0.50	0.96	1.69	0.40	1.36	0.51	1.15
<i>MIF</i>	0.22	0.81	1.37	1.73	0.43	0.98	1.60	0.17	1.06	0.75	0.91
<i>MUD</i> (cm)	0.49	1.65	1.74	1.96	0.64	1.19	1.83	0.58	1.59	0.73	1.24
<i>T_s</i>	0.74	1.58	1.72	1.92	0.38	0.63	1.14	0.10	0.50	0.17	0.89
<i>D_{SMV}</i>	0.34	0.11	0.65	1.59	0.41	1.04	1.74	0.27	1.15	0.50	0.78
<i>D_{RMS}</i>	0.24	0.12	0.90	1.72	0.56	1.30	1.85	0.51	1.47	0.50	0.92
<i>D_{BC}</i>	0.38	0.04	0.59	1.62	0.37	1.11	1.86	0.37	1.35	0.47	0.82
<i>D_{PS}</i>	0.12	0.06	0.75	1.42	0.30	1.12	1.65	0.46	1.16	0.33	0.74
<i>D_{RS}</i>	0.28	0.06	0.15	0.66	0.27	0.81	1.50	0.27	0.95	0.25	0.52
<i>l_{SMV}</i> (cm)	0.82	1.61	1.70	1.87	0.38	0.82	1.35	0.35	0.96	0.25	1.01
<i>l_{RMS}</i> (cm)	0.85	1.10	1.03	0.93	0.04	0.02	0.01	0.00	0.04	0.02	0.40

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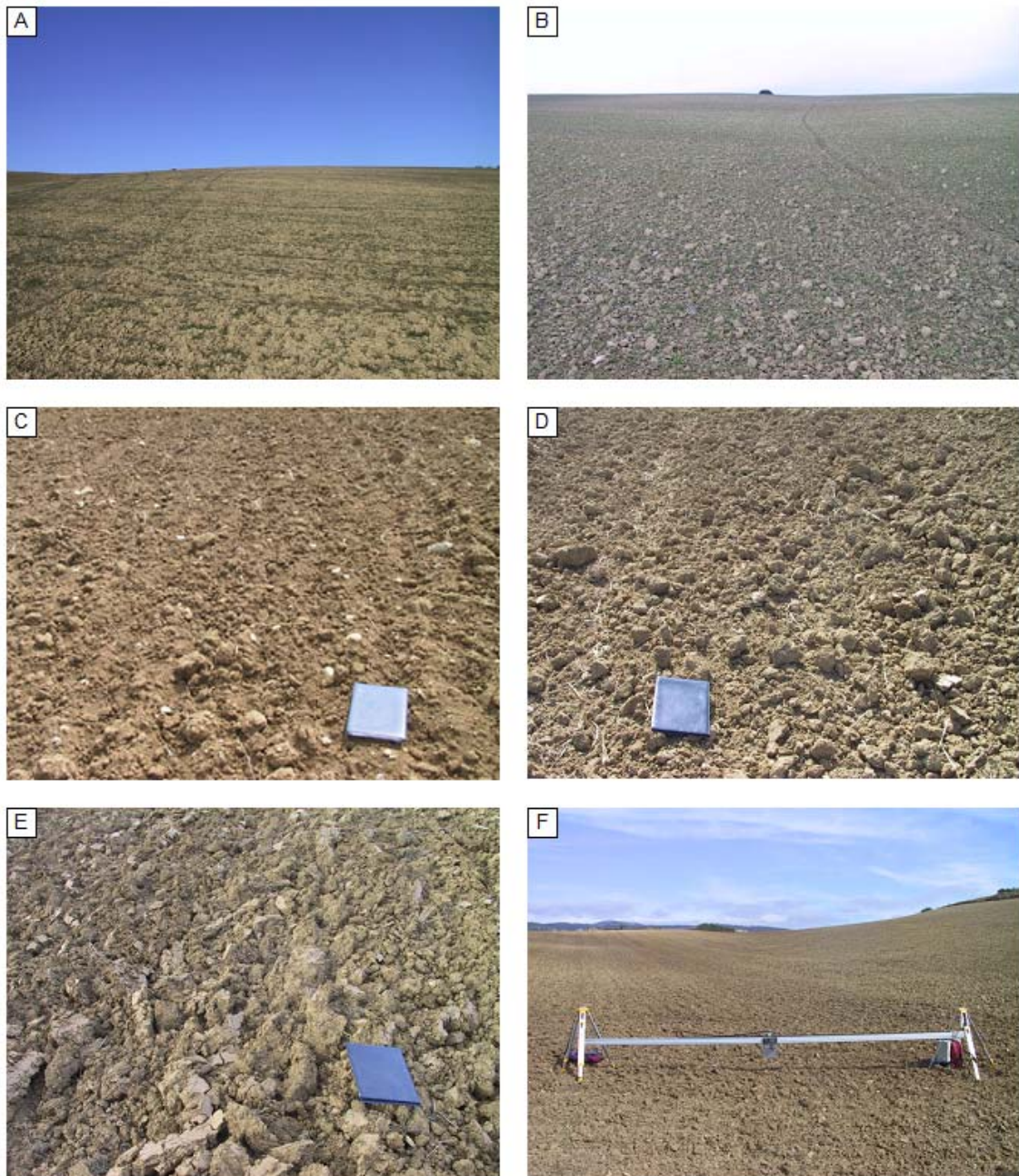
1 **Figure list and captions**

2 Figure 1. Examples of surface roughness triggered by agricultural treatments; (A)
3 planted modified by rainfall, (B) planted unmodified, (C) harrowed smooth, (D)
4 harrowed rough and (E) mouldboard plough; and (F) profilometer used for data taking.
5 As a reference, the notebook in C, D, and E is 30 cm long; and 5 m the length of the
6 profilometer bar in F.

7 Figure 2. Examples of height profiles of each of the roughness classes studied.

8 Figure 3. Box diagrams per roughness classes of the estimated values of the different
9 parameters.

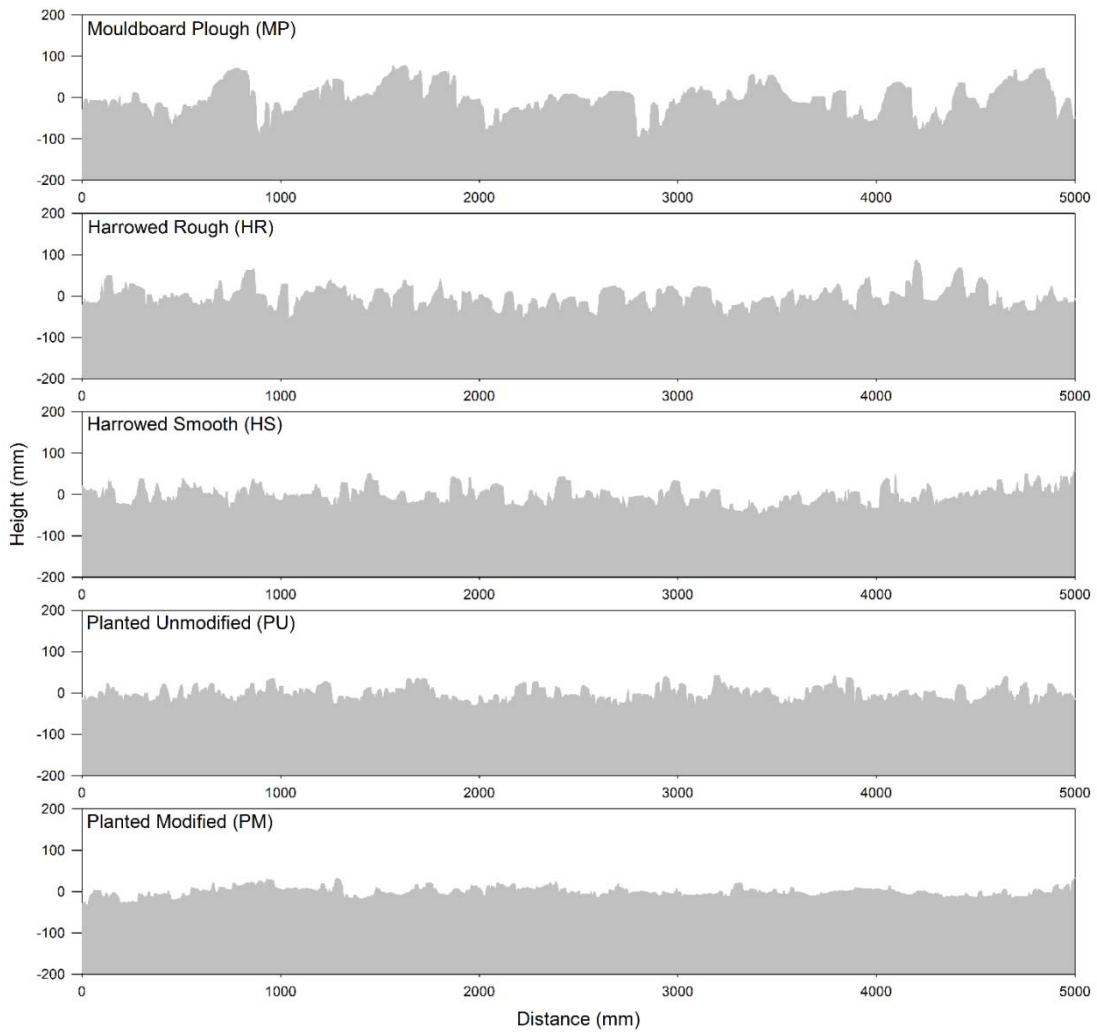
10 Figure 4. Spearman correlation matrix of the roughness parameters (n=164).



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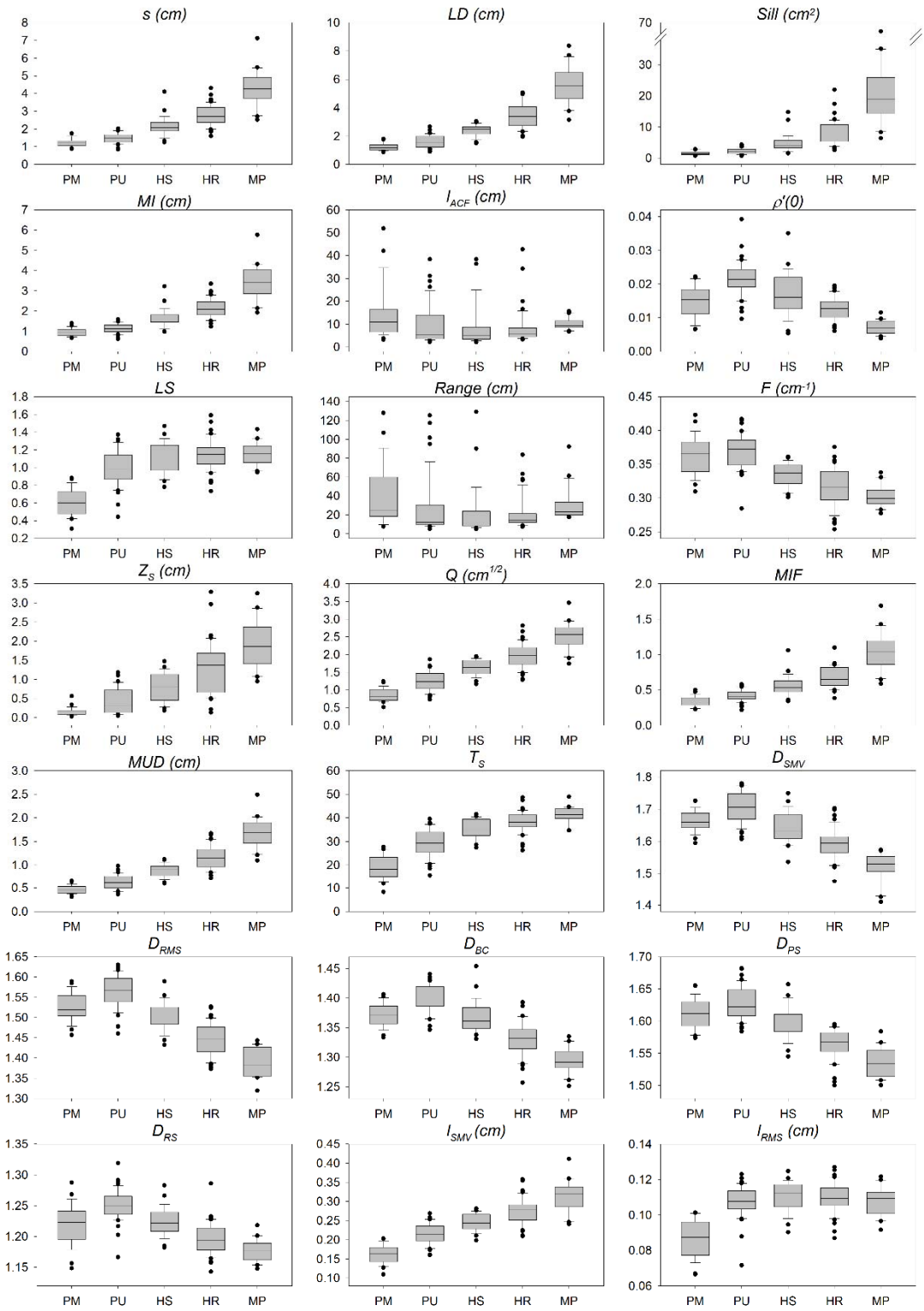
6



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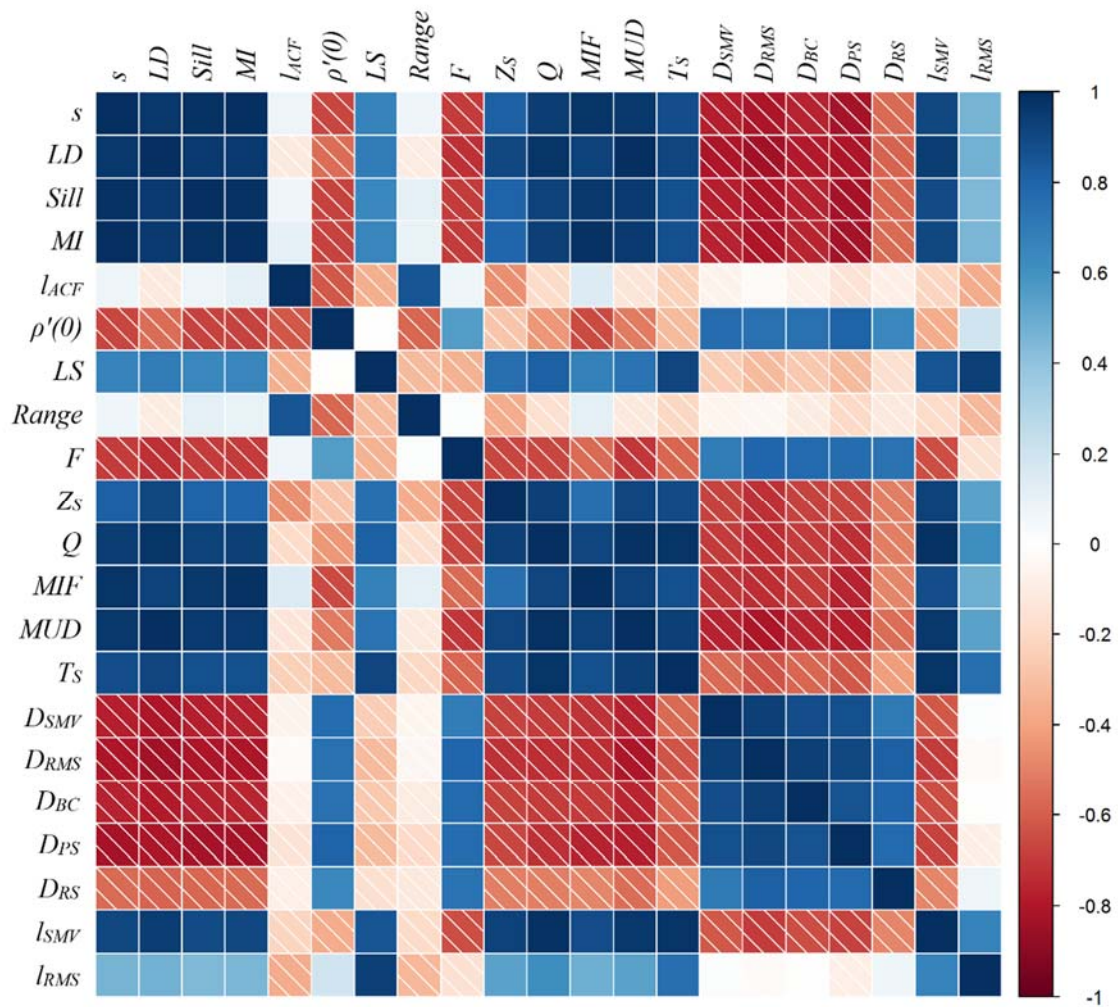
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