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Evidence for the synthesis of La-hexaaluminate from aluminum-containing saline slag wastes: correction of structural defects and phase purification at low temperature

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Abstract

The synthesis of a lanthanum hexaaluminate from the aluminum extracted from a saline slag waste is presented for the first time. Briefly, a reducing 2 M solution of HCl is used to extract the aluminum, giving 8.9 $g_{Al}/c'm^2$ along with other metals in lower concentrations. This solution is used to synthesize the hexaaluminate by mixing with a stoichiometric amount of lanthanum nitrale. The results showed the formation of pure phase hexaaluminate at 1473 K, as well as predominance of the hexaaluminate phase at temperatures of 1273 and 1373 K. Here results also indicate that the pure hexaaluminate phase can be obtailed at a much lower temperature than when commercial aluminum solutions are used improving the applications as catalyst and thermal barrier material. It was the pure found that the presence of other metals in solution allows the structural proviems and purity of the La-hexaaluminate phase to be corrected when working with stoichiometric ratios.

Keywords: aluminum industrial wastes, waste valorization, hexaaluminate, saline slags

1. Introduction

Aluminum is a non-ferrous metal used in a large number of applications and in a wide range of products. However, unlike other metals, aluminum can be almost completely recycled into new products by melting [1]. When these melting processes are carried out on an industrial scale, tilting rotary furnaces and salts are used. This results in the generation of saline slag wastes, which are classified as hazardous wastes [2,3]. The composition of these saline slags depends on the quality of the material being recycled and the amount of salt added to the furnace. In general, three fractions can be differentiated in saline slags, namely salts (NaCl + "Cl), aluminum metal and a fraction of non-metallic oxides. Recovery of the waste involves separating each of these fractions and providing them with an applicatio 1, 5]. The non-metallic oxides fraction has been found to contain Fe₂O₃, SiO₂, Na₂O, AIN, Al₂O₃, NaCl, MgO, Al₂O₃, traces of KCl, cryolite (Na₃AlF₆), aluminum ca. bid ϵ (Al₄C₃) and small amounts of fluoride and chloride. Additionally, the presence of other components, such as MgF_2 , NaAlCl₄, KAlCl₄, MgO, KMgF₃ and K₂Na (F₆, inas also been reported [2,5-7]. The aluminum present in the slags ca: by extracted by alkaline or acid leaching to synthesize other interesting materials such as zeolites and layered double hydroxides, developed by our research group [c 10]. In the case of acid leaching, which involves treatment with HCl at low concentrations, several species, such as Al³⁺, Fe³⁺, Ca²⁺, Mg²⁺, Na⁺ and chlorides, amongst others, can be extracted in solution [2,6].

Hexaaluminates are a family of hexagonal aluminate compounds that have a unique layered structure comprising alternating spinel blocks with closed packed array of oxide ions and mirror planes. The general formula is $AB_xAI_{12-x}O_{19}$, where A can be a cation such as Na, Ba, La, Ca, Sr, Ce, amongst others. Component *B* represents a transition metal (Mn, Fe, Co, Cu, Ni, etc.) or noble metal ion (Ir, Ru, Pd, Rh), which can partially or completely replace the Al positions in the crystallographic structure [11,12]. The spinel blocks are composed only of Al³⁺ and O²⁻ ions and have the same rigid structure as the spinel. Large cations such as Na⁺, K⁺, Sr²⁺ and La³⁺ are found in the spacious mirror plane. The charge and radius of these cations mean that hexaaluminates have a β -Al₂O₃ or magnetoplumbite (MP)-type structure [13].

Several methods for the synthesis of hexaaluminates have been reported: solid state reaction [14,15], sol-gel [14,16,17], co-precipitation [18,19], reverse

microemulsion [20,21], nitrate decomposition [22-24], hydrothermal synthesis [25], carbon template [26,27], freeze drying [28,29], among others. The decomposition of nitrates is a simple method, since it consists of adding the aqueous solutions of the salts to a mixture of polyethylene glycol-isopropanol, after a reaction time, which may be under pressure, the drying and calcination steps are continued. Based on this method, the synthesis of hexaaluminates from an aluminum solution extracted from saline slag wastes is developed in this work.

Hexaaluminates have been used as catalytic supports for several reactions, such as combustion of VOCs, partial oxidation and dry reforming of methane, amongst others [30-33], with catalytic behaviors and properties being reported in terms of yield, selectivity and stability. Lanthanum hexaaluminate ('HA) has a high resistance to deactivation by coke deposition, and has therefore then suggested by several authors to be a very interesting catalyst for the above time of reactions [11,18,22,34]. Other applications of great interest for this type of material are as ceramic coatings and, recently, as a thermal barrier in turbines and yet engines in aircraft. Due to its thermal stability at high temperature and ageinst hot corrosion, it is an alternative material to the zirconium typically used in the processes [35-37].

In this work, aluminum extracted from saline slag wastes using aqueous HCl solutions is used as an alternative aluminum source for the synthesis of hexaaluminates for the first time. The aluminum solutions were used as precursors in combination with lanthacture to obtain hexaaluminates with a molar La/Al ratio of 1:11. The presence of other metals in the extracted solution means that the hexaaluminate structure can be formed at a lower temperature than that reported when Al and La from commercial solutions are considered.

2. Experimental

2.1. Materials and aluminum extraction

Lanthanum(III) chloride heptahydrate (99.9%, Sigma Aldrich), 2-propanol (99.5%, Sigma Aldrich) and polyethylene glycol 400 (Merck) were used.

Aluminum was extracted from saline slags using the following procedure: 50 g of saline slag was added to 750 cm³ of an aqueous reagent solution (HCl 2M) in a reflux system consisting of a 1000 cm³ erlenmeyer flask with tube condenser, thus avoiding

volume losses. The slurries were heated to 373 K and kept at that temperature for 2 h. The solution was then allowed to cool and separated by centrifugation. The most important constituents of the filtered solution were determined by ICP-OES, using a VARIAN ICP-OES VISTA MPX with radial vision. The results obtained are summarized in Table 1. The composition of the aluminum saline slags before extraction (see Table 2) was determined by X-ray fluorescence (XRF), (through calibrated lines using well-characterized international minerals and semiquantitative for La through the measurement of a set of scans) in a PANalytical AXIOS instrument. For these results, low limits of detection for major elements were in the range of 0.01 wt.%, and approximately 10 ppm for trace elements.

2.2. Hexaaluminate synthesis

Based on the nitrate decomposition method and hydrothermal synthesis, our research group has developed the synthesic method described below, denoted as Alcohol Dilution (AD), in which 250 mL of the acid solution with aluminum extracted from the saline slags was concentrated erving as a matrix where the other reagents are added. The extracted aluminum solution was heated to reduce its volume fivefold (50 mL), thus giving a concentrated erving for hexaaluminate synthesis. A quantity of lanthanum chloride corresponding to a molar La/Al ratio of 1:11 was dissolved in 200 mL a mixture of isopropano, 'nolyethylene glycol in a 1/1 volumetric ratio. The mixture of alcohols was added to the aluminum solution slowly, with vigorous stirring, over 30 minutes, then poured into a 250 mL stainless steel autoclave reactor and heated at 473 K for 16 h. The reputting product was dried in an oven until the liquid matrix had been eliminated, then calcinated at a heating rate of 10 K/min to 673 K for 1 h, and then successively to several temperatures between 873 and 1473 K for 2 h to study the structure evolution.

2.2.1. Characterization techniques

The structural phases were analyzed using an X-ray diffractometer (model Siemens D5000) equipped with an Ni-filtered CuK α radiation source (λ = 0.1548 nm). The main textural properties of the solids were determined by nitrogen adsorption at 77 K using a Micromeritics ASAP 2020 Plus adsorption analyzer. The chemical

composition of the sample was determined semiquantitatively by X-ray fluorescence (XRF) using a PANalytical AXIOS instrument. The programmed reduction temperature was measured using a Micromeritics TPR/TPD 2900 device and the infrared spectra of the samples calcined at several temperatures using a Jasco FT/IR-4700 spectrometer. Finally, the morphological analysis and chemical composition of the sample were carried out using a SEM Phenom Pro Desktop and an HR-TEM JEOL JEM 2100F.

3. Results and discussion

The material synthesized using La and aluminum extrected from saline slags, and calcined at 1473 K, was characterized by XRD and the pattern obtained is shown in Figure 1. According to the extraction of multimetal oxides, and the presence of La and Ca, the most probable hexaaluminate structure, and that which best fits the existing patterns, appears to be magnetoplumbite. Indeed, hibonite-Ca (pattern # 00-007-0785), which is a type of magnetoplumbite, is the structure in closest agreement with the synthesized sample.

The hexaaluminate synthesized v. 's calcined at various temperatures to evaluate how the structure evolves with temperature. The X-ray diffractograms of the samples at several temperatures are also presented in Figure 1. Thus, the sample calcined at 873 K (a) presents an amorpheus phase that appears to be similar to minerals from the spinel group of alumine (pettern # 00-021-1152), most likely due to the presence of a mixture of MgO, MnC and reO, with Al₂O₃. Upon calcination of the sample at 1073 K (b), the spinel and the additional metal oxides begin to transform into the hexaaluminate phase hibonite-Ca (pattern # 00-007-0785), as shown by the appearance of diffraction lines related to this oxide. Calcination at 1273 K (c) results in a decrease in the intensity of the diffraction lines for the spinels seen at lower temperatures and an increase in the intensity of the hexaaluminate peaks. The diffractograms for samples (b) and (c) are complex due to the mixture of components and crystallographic phases. For sample (d), which was calcined at 1473 K, the spinel phase has disappeared almost completely and high correspondence with the hexaaluminate is found. As such, the hexaaluminate has almost completed its

transformation at this temperature since the diffraction lines obtained are well defined.

LHA exhibit a double Frenkel defect, which hinders formation of the hexaaluminate phase with a molar La:Al ratio of 1:11. This defect can be corrected if the amount of aluminum is increased to around 14-15 with respect to lanthanum. As such, a predominant hexaaluminate phase can be obtained, with an aluminate phase as a secondary, although not pure, phase even when increasing the calcination temperature to 1723 K [38,39]. Rao and Mariappan [38] studied the structural formation of LHA, comparing two synthesis methods and using molar La:Al proportions of 1:11, 1:12 and 1:15. Samples were calcined at 1723 r Spr 2 h, obtaining a high crystallinity with very well defined peaks in all three cases. The aluminate phase was found to be predominant for the molar ratios 1:11 and 1:12, with the hexaaluminate phase being secondary. In the case of the sample ob ained with a 1:15 molar ratio, a predominant hexaaluminate phase was observed, with the aluminate phase being secondary in this case. No pure phases were clatained at this temperature. Park et al. [39] showed that LHA is more likely t br a non-stoichiometric phase corresponding to La_{0.83}Al_{11.83}O₁₉ or LaAl_{11.67}O₁₉ with molar Al/La ratio in the range 13-14. These authors also predicted that these two press, which have an MP structure, may form solid solutions. Modeling also revealed the possible existence of metastable phases. They explained the structural detect observed using two types of defect models: a "vacancy model" and an "interstitue" or ygen model" [39].

In the case of the Aexaaluminate obtained from the saline slags using a molar La:Al ratio of 1:11, a rure phase with high densification of the solid was obtained at 1473 K. This finding shows that the saline slags solution self-corrects the double Frenkel structural defect. A stoichiometric ratio, and the metallic synergy of the components, makes it possible to obtain the hexaaluminate phase at lower calcination temperatures. This may be due to the fact that a lower diffusion energy is needed in the solid-state reaction in the presence of other metals. Acid treatment of the saline slags allows other metals, such as Mg, Fe, Si, Mn and Ti, which work in excellent synergy with La to obtain the hexaaluminate, to be extracted.

In order to corroborate that the hibonite autocorriges the structural defect Frenkel in LHA, two samples with commercial precursors were synthesized and calcined at 1473 K for 2 h. The samples were AD1, mole La/Al ratio of 1:11, and AD2, mole La/Al/Ni ratio of 1:15:0.25. The XRD patterns are included in Figure 2. It can be seen that the hexaaluminate structure is not achieved when using a mole La/Al ratio of 1:11 (AD1). Under these conditions, the predominant phase is La(AlO₃) due to the vacancies generated by the double Frenkell effect in LHA, possibly due to the repulsive effects of La³⁺ on Al³⁺ that prevents it from migrating within the structure and to form a hexagonal arrangement corresponding to the LHA phase. On the contrary, it can also be seen that the hexaaluminate phase develops for sample AD2. This result can be explained by the presence of an excess of Al^{3+} and Ni^{2+} . The addition of nickel allows the formation of the MP-type hexaaluminate structure and reduce the secondary phases of aluminate to 1473 K, an effect reported by Rao and Mariappan [38]. This result demonstrates the synergistic effect of metals and the correction of the defect by using Al extracted from saline slags, since other metals that carry this effect are also extracted.

The quantitative chemical composition by of the sample synthesized, as determined by FXR (low limits of detection for major elements are in the range of 0.01 wt.%, and approximately 10 pom for trace elements) and SEM-EDX (determined by EDX-mapping from an average of 20 measurements on the sample with a percentage measurement uncertained or 0.5 wt.%), is shown in Table 3 and Figure 3. These values allow an atomic relationship between the main elements that may be present to be established. The table shows a possible composition in groups according to the general hexaaluminate formula AB_xAl_{12-x}O₁₉, where A represents cations such as La, Ca, Na and B represents metals that replace Al in the structure, such as Mg, Fe, Si, Ti and Mn. The hibonite formula shown in Equation 1 can therefore tentatively be proposed, assuming that this oxide is only obtained in the final sample. Although the sum of cations (A) in the hibonite formula must be 1, and a value of more than 2.29 is obtained, this may be possible in the case of hexagonal structures with values of metallic cations greater than 1 due to the presence of cations such as Ca and Na. The formation of Ca₂Al₁₂O₁₉ has recently been proposed via a solid-state reaction [40-42]. In addition, Fe can

replace AI completely in a hexaaluminate and convert it to hexaferrite [12,43], therefore both structures could be comparable. In the case of hexaferrites, several examples of structures containing large cations with molar ratios greater than 1, such as Ba₂Fe₁₂O₁₉ [44,45], Ba₂Cu₂Fe₁₂O₂₂, Ba₂Fe₂Fe₁₂O₂₂ (type Hexaferrite Y) [44-47], which still remain in the hexagonal phase, are known.

 $(Ca_{0.54}Na_{0.67}La_{1.08})(Si_{1.32}Mg_{0.83}Fe_{0.18}Mn_{0.02}Ti_{0.03})Al_{9.06}O_{19-\delta}$

(Equation 1)

The specific surface and pore volume values at several temperatures, and the predominant phase at those temperatures, can be found in Table 4. The S_{BET} results at 1473 K suggest that almost complete sintering is exhibited as a result of the applied synthesis mechanism, thus resulting in a high densification. It is important to mention that the predominant hexaluminate phase is observed at 1373 K, with excellent purity and acceptable porosity for use as catal, the support, thus representing a reduction in the formation temperature. The size of the crystallite was determined using the Debye–Scherrer equation. Evolution of the crystallite size was observed, with uniform growth of the crystallite, thus confirming an excellent densification. In addition, a sintering process that occurs at very low temperatures can be proposed, since the process starts with a low S_{BL} -value compared to alumina and a small crystallite size. As such, the synergy of the same slag components may benefit diffusion of the species, thus resulting in high densification, high diffusion in the solid state and low porosity, which allows the phase transformation to occur at a lower temperature.

The decrease in porosity with calcination temperature is shown in Figure 4, and the corresponding changes in transformations of the spinel phases become clear when applying the derivative of the curve. It can also be seen that the enrichment range of the LHA phase occurs between 1273 and 1373 K, where the derivative remains almost constant, whereas the slope changes completely at the temperature at which the pure phase appears (1473 K).

When La reacts with other metals it exhibits different structural mechanisms in the synthesis of hexaaluminates, with these mechanisms being conditioned by the

nature of the metals, as well as by the stoichiometric ratio in which they are present. This has a significant effect on the structure of the final material, the temperature required to form it, the type of phase that is formed, as well as on the textural properties. This behavior was proposed and discussed by Zhang et al. [12], who studied the evolution of the crystal structure with temperature and the crystallographic centers of LaFe_xAl_{12-x}O₁₉-type hexaaluminates synthesized using a co-precipitation method with commercial precursors. These authors modified the Fe concentration (x = 0-12) and calcined the materials at several temperatures (between 973 and 1673 K), finding various phase compositions with variations in the Fe concentration, which competes with AI at the structural centers. Thus, for a value of x = 0, they found MP/LaAlO₃ as phases, whereas for a value of x betwee 1 and 7 they observed the MP phase, for a value of x between 8 and 11 MP/ α -Fe₂C₅ phases and, finally, for a value of x = 12 they found α -Fe₂O₃/LaFeO₃ phases. They also proposed that Fe is able to substitute Al in the spinel block. The same authors [48] synthesized the hexaaluminate BaFe_xAl_{12-x}O₁₉ by varying the Fe concentration (x = 0.12) and found that the structural phase was transformed from β -Al₂O₃ \circ N₁P as the Fe concentration increased.

Machida et al. [49] and Groppi et al. [50] investigated $BaMn_xAl_{12-x}O_{19}$ catalysts and found that replacement of a'un from with manganese up to $x \approx 3$ was possible and that additional phases, such as perosvkite, spinel, etc., are produced if this ratio is increased. Wang et al. [51, and Tian et al. [13] studied substituted materials and obtained LaMn_xAl_{12-x}O_{19} with a maximum value of x = 1. They also found that LaMnO₃ formation occurred ofter the addition of additional Mn. This behavior may be associated with the limited ability of hexaaluminate to incorporate other metal ions into the structure.

The relationship between the decrease in porosity and crystallite size are shown in Figure 5 (a), which allows the effect of the phase transformation on the specific surface to be identified since the spinel phase undergoes changes towards the hexaaluminate phase. In the solid matrix, the competition between species such as Fe-Al to occupy the same structural centers generates this inverse correspondence between the crystallography and the textural properties for the hexaaluminate synthesized. This same phenomenon was observed by Zhu et al. [48], who reported that the variation in Fe concentration in BaFe_xAl_{12-x}O₁₉ generates a destructive effect

on porosity related to competition for the aforementioned octahedral centers, finding specific surface values of between 20 and 4 m^2/g for values of x between 0 and 9. For values of x greater than 9, the specific surface is zero.

The relationship between specific surface area and crystallite size and temperature are also shown in Figure 5 (b), which was created using the Krigin–Gridding interpolation method and according to the following model (Equation 2):

$$S_{BET} = \frac{846.189 - 0.667T + 24.577SG - 6.4677SG^2 + 0.3604SG^3}{1 - 0.01516T + 5.6945T^2 - 3.6677T^3 + 1.2670SG - 0.03177SG^2}$$
(Equation 2)

where T is the calcination temperature and SG the crystal ite size. This model gives an R^2 value of 0.992 and a χ^2 value of 1.05, thus showing the model fits the data very well.

The reduction profiles of the hexaaluminates calcined at various temperatures are shown in Figure 6. It can be seen that materials calcined at 873 and 1073 K present reduction processes over a wide temperature range (between 570 and 1173 K), with this behavior being related to the reduction of species that have not yet been incorporated into the hexaaluminate structure. Once the hexaaluminate phase has formed and predominates, in ot're words for samples calcined above 1273 K, there is no evidence of reduction processes. These findings indicate that there are no reducible species outside the structure and that the Fe and Mn extracted from the starting saline slags (see Table 2) have been fully incorporated into the hexaaluminate structure. It should also be noted that the reducible oxides that contribute to H_2 consumption are those related to Fe species, and to a lesser extent to Mn species, given that La, Al, Ca and Mg oxides are not reducible. The reduction profile of the sample calcined at 873 K shows four reduction maxima at 593, 713, 773 and 913 K. The first can be attributed to the reduction Mn_2O_3 to Mn_3O_4 , the second to the reduction of Mn_3O_4 to MnO and Fe_2O_3 to Fe_3O_4 , and the third to the Fe species that migrate from Fe_3O_4 to FeO. Finally, the latter corresponds to the transition from FeO to metallic Fe since MnO is not reducible under these conditions [52,53]. The sample calcined at 1073 K shows the typical behavior described by Leith and Howden [53] for materials based on Fe and Mn oxides. In this case, the species are reduced at higher temperatures due to interactions with the metallic support. In view of the temperature profile, reduction maxima can be

assigned to the temperatures 713, 780, 876 and 995 K. The correspondence of species would be with those described above.

The evolution of the structure of the hexaaluminate as a function of calcination temperature was also characterized by FTIR and is shown in Figure 7, which shows a broad band centered at 3440 cm⁻¹ and another at 1640 cm⁻¹ assigned to the characteristic stretching and bending vibrations of OH groups, respectively. These bands are associated with water adsorbed on the samples, and experience a decrease in intensity with increasing calcination temperature, which may be related to the loss of surface area inherent to the process [54]. All spectra shows bands in the range 400-1000 cm⁻¹ assigned to the vibration of metal-oxygen bon is (M-O). In the presence of multiple metals, the increase in calcination temperature means that hexaaluminate structure formation results in narrower and better defined bands [54,55]. In all cases, bands due to tetrahedral [AIO₄]⁵⁻ stretching vibrations, specifically the shoulders in the spectra at 750 cm⁻¹, are evidence of this kind of site. Octahedral [AlO₆]⁹⁻ stretching vibrations appear at 695 cm⁻¹ and as a she lloc. at 578 cm⁻¹ [54,55]. Bands due to M-O bonds other than to Al can be obcarved in the spectra, including the Mg-O bond vibration at 840 cm⁻¹ [55], Fe-O at 155 cm⁻¹ [55-57], and, finally, the sample calcined at 1473 K exhibits characteristic reck for hibonite La-Ca at 520, 660 and 980 cm⁻¹ [55,58].

The SEM-TEM image of the hexaaluminate calcined at 1473 K is shown in Figures 3 and 8. From Figure 3, there are an agglomeration of the hexaaluminates which causes a high decisication and a low porosity [59]. It is not observed that the microcrystals are sintered since they keep their microstructure very well defined and independent of each other. In the diffractogram included in Figure 1, a high crystallinity of the sample was observed, which could be related to the excellent structural definition that can be seen. In addition, an aluminate secondary phase was practically not observed, which would allow establishing a high phase purity, conditioning with the SEM images and with the composition determined by EDX mapping (20 measurements on the sample and an average composition with a percentage uncertainty of the measurement of 0.5%). TEM-SAED images of the hexaaluminates obtained are also included in Figure 8. In this figure is possible to see

the atomic distribution of the hexagonal arrangements in the microstructure and the interplanar lattice patterns corresponding to LHA.

4. Conclusion

The synthesis of hexaaluminate and La-Ca hibonite from aluminum extracted from an aluminum saline slag has been presented for the first time. The proposed procedure is suitable for upgrading a hazardous industrial waste and obtaining a material that can have various uses as a catalyst and thermal insulator.

The aluminum used in the synthesis of hexaaluminate is extracted from saline slags in an acid medium, a process that allows the extraction of smaller quantities of other metals. The presence of these metals provides great advantages in the synthesis of hexaluminates since it allows to obtain the hexaaluminate phase with a stoichiometric La/Al ratio at lower temperaters. The another hexaaluminates reported, and with a greater degree of phase purity than if the synthesis is carried out using commercial reagents.

Credit authorship contribution statement

In this work, Mr J.J. Torrez decrera carried out the experiments, analyzed results and involved in writing/revising manuscript; Dr E.G. Fuentes-Ordoñez and Prof S.A. Korili analyzed results and incolved in writing/revising manuscript; Prof. A. Gil provided conceptualization, projected ministration, manuscript writing and revision guidance.

Declaration of competing interest

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

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Solution of the second second

Captions

Table 1. Chemical composition of the solution after acid extraction.

- Table 2. Chemical composition of the aluminum saline slags before aluminum extraction.
- Table 3. Chemical composition of the La-hexaaluminate synthesized.
- **Table 4.** BET specific surface areas, pore volumes and crystallite sizes of the samplesynthesized at several temperatures. The structure of the phase thatpredominates at each temperature is also included.
- Figure 1. (A) XRD pattern of the hexaaluminate synthesized using La and Al extracted from saline slags, AD method (the hibeline pattern is included for comparison). (B) XRD patterns of the hexaaluminate calcined at several temperatures and evolution of the phaces. (a) 873 K, (b) 1073 K, (c) 1273 K, and (d) 1473 K. Symbols: ▼ Spinel pattern 00-021-1152, ▼ Hibonite pattern 00-007-0785.
- **Figure 2**. XRD patterns of sample synthesized with commercial precursors (AD method) and calcined at 1473 k for 2 h (various patterns are included for comparison). AD1, molar La/Al ratio of 1:11, AD2, molar La/Al/Ni ratio of 1:15:0.25.
- Figure 3. SEM micrographs and EDX-mapping analysis of the hexaaluminate synthesized at 173 K. The mass surface and the atomic concentrations are also included
- **Figure 4.** Evolution of S_{BET} with calcination temperature.
- **Figure 5.** (A) Evolution of S_{BET} with crystallite size. (B) Krigin Gridding interpolation.
- Figure 6. TPR patterns of the hexaaluminate calcined at several temperatures.
- Figure 7. FTIR spectra of the hexaaluminate calcined at several temperatures.
- Figure 8. TEM-SAED images of the hexaaluminate synthetized at 1473 K. The superficial patters and he interplanar distances in the structure can be observed.

Composition	AI	Fe	Са	Mg
g/cm³	8.96 ± 0.13	0.85 ± 0.01	0.76 ± 0.01	0.49 ± 0.01

Southand

extraction.									
Composition	Na ₂ O	MgO	Al ₂ O ₃	SiO ₂	P ₂ O ₅	SO ₃	Cl	K ₂ O	CaO

55.23 4.23

0.07 0.41 0.47 0.50 2.12

0.77

6.49

wt.%

Table 2. Chemical composition of the aluminum saline slags before aluminum
extraction.

Composition	TiO ₂	Cr	MnO	Fe ₂ O ₃	Ва	Cu	F	Zn	
wt.%	0.65	0.07	0.26	1.25	0.07	0.51	0.41	0.17	

		Α				B _x			Al _{12-x}	Ο _{19-δ}
Oxides	La ₂ O ₃	CaO	Na ₂ O	MgO	Fe ₂ O ₃	Si ₂ O	Ti₂O	MnO	Al ₂ O ₃	0
wt. %	20.49	3.52	2.40	3.90	1.67	9.25	0.34	0.28	56.91	
mol. %	7.57	3.78	4.66	5.82	1.26	9.27	0.26	0.19	67.19	
Atom	La	Са	Na	Mg	Fe	Si	Ti	Mn	Al	0
LHA composition	1.08	0.54	0.67	0.83	0.18	1.32	0.03	0.02	9.06	19-δ

Table 3. Chemical composition of the La-hexaaluminate synthesized.

Table 4. BET specific surface areas, pore volumes and crystallite sizes of the sample synthesized at several temperatures. The structure of the phase that predominates at each temperature is also included.

Temperature (K)	S _{BET} (m²/g)	Vp (cm ³ /g)	Crystallite size (nm)	Phase structure
873	59	0.216	3.52	Spinel
1073	28	0.154	3.97	Spinel >> LHA
1273	17	0.056	5.30	LHA >> Spinel
1373	9	0.056	8.70	LHA >> Spinel
1473	1	0.003	9.07	LHA

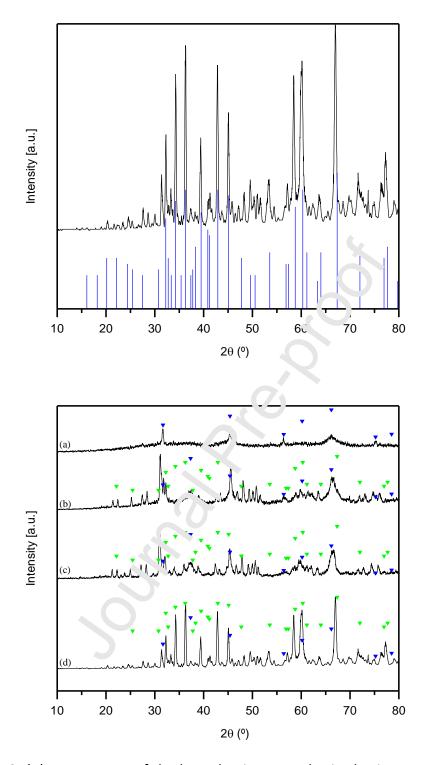


Figure 2. (A) XRD pattern of the hexaaluminate synthesized using La and Al extracted from saline slags, AD method (the hibonite pattern is included for comparison). (B) XRD patterns of the hexaaluminate calcined at several temperatures and evolution of the phases. (a) 873 K, (b) 1073 K, (c) 1273 K, and (d) 1473 K. Symbols: $\mathbf{\nabla}$ Spinel pattern 00-021-1152, $\mathbf{\nabla}$ Hibonite pattern 00-007-0785

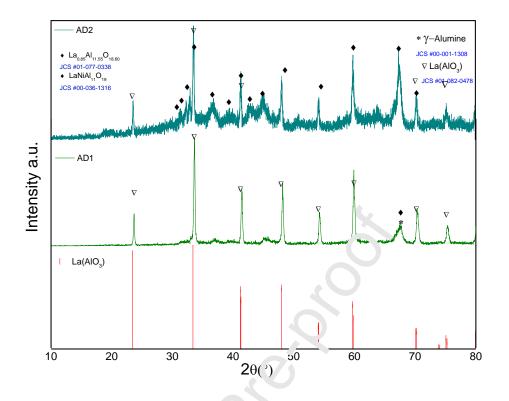
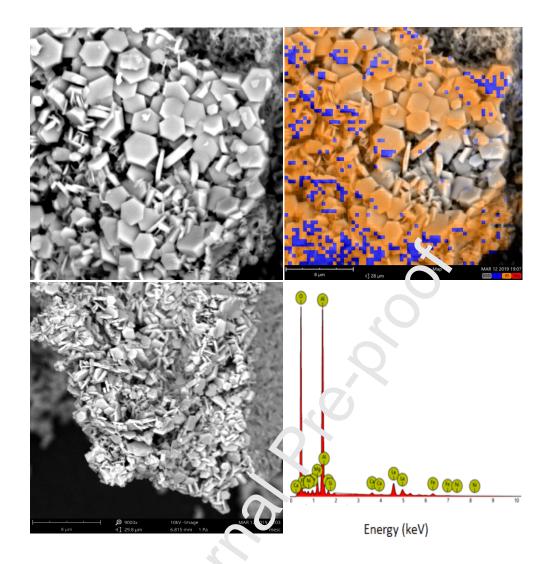


Figure 2. XRD patterns of sample switchesized with commercial precursors (AD method) and calcined at 1473 K for 2 h (various patterns are included for comparison). AD1, molar La/Al ratio of 1:11, AF/2 molar La/Al/Ni ratio of 1:15:0.25.



	0	1	La	Mg	Fe	Na	Si	Са
% mass concentration	36.29	30)6	25.56	2.44	2.35	0.93	0.78	0.59
	±0.18	± 0.15	±0.12	±0.01	±0.01	±0.005	±0.004	±0.003
% atomic	59.35	29.95	4.8	2.62	1.1	1.06	0.73	0.38
concentration	±0.30	±0.15	±0.02	±0.01	±0.006	±0.005	±0.004	±0.002

Figure 3. SEM micrographs and EDX-mapping analysis of the hexaaluminate synthesized at 1473 K. The mass surface and the atomic concentrations are also included.

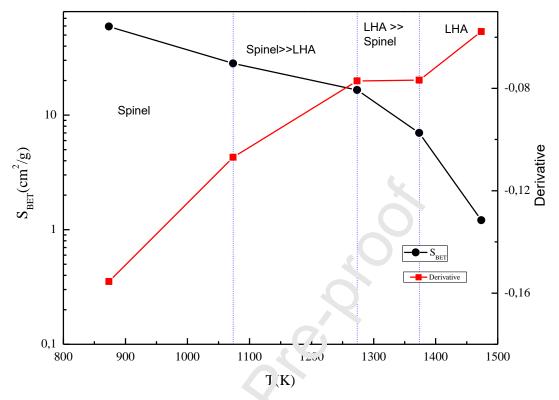


Figure 4. Evolution of S_{BET} with calcination temperature.

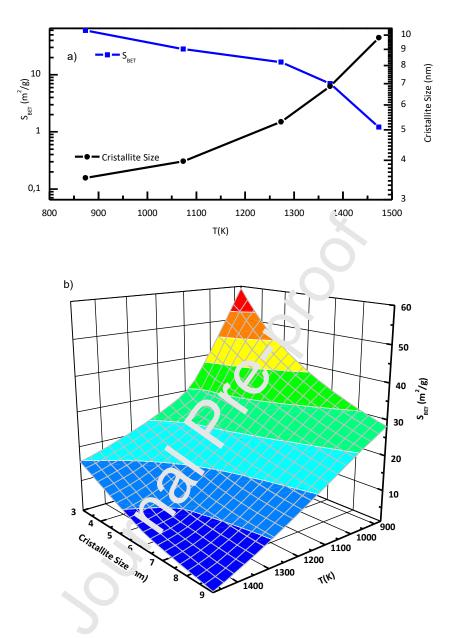


Figure 5. (A) Evolution of S_{BET} with crystallite size. (B) Krigin Gridding interpolation.

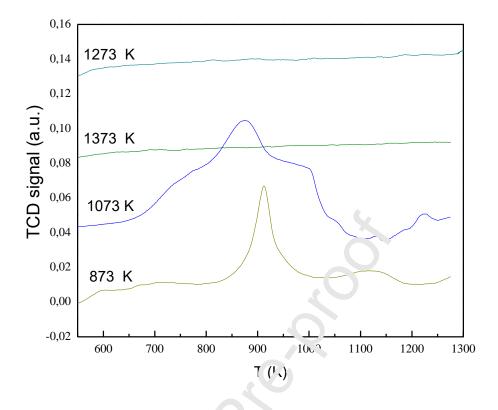


Figure 6. TPR patterns of the hexaaluminete calcined at several temperatures.

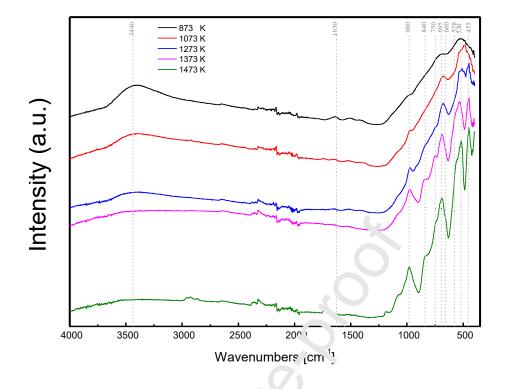


Figure 7. FTIR spectra of the hexaalum ina e colcined at several temperatures.

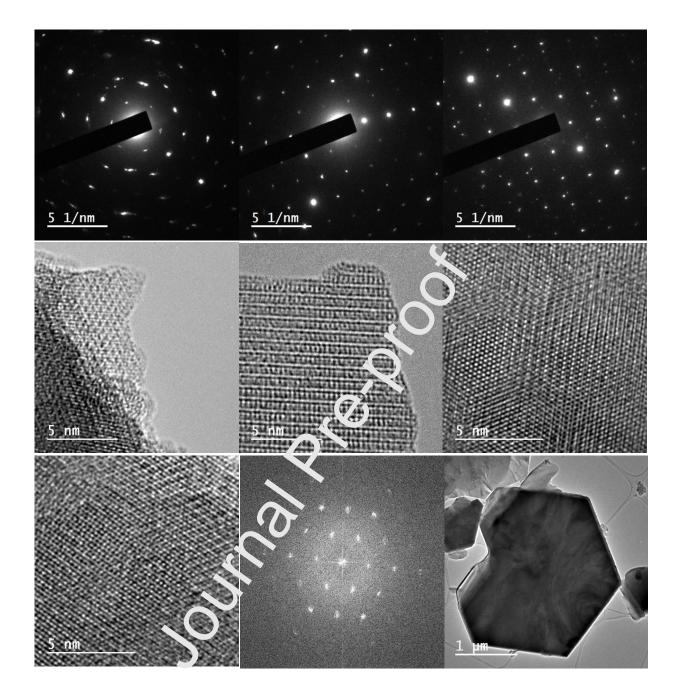


Figure 8. TEM-SAED images of the hexaaluminate synthetized at 1473 K. The superficial patters and he interplanar distances in the structure can be observed.

Credit authorship contribution statement

In this work, Mr J.J. Torrez-Herrera carried out the experiments, analyzed results and involved in writing/revising manuscript; Dr E.G. Fuentes-Ordoñez and Prof S.A. Korili analyzed results and involved in writing/revising manuscript; Prof. A. Gil provided conceptualization, project administration, manuscript writing and revision guidance.

Author declaration

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- ▶ Pure phases of La-hexaaluminates at low temperature from saline slags were obtained.
- ► Acid aluminum extracted from saline slags was used in the synthesis of La-hexaaluminates.
- ► The synthesis of hexaaluminate from an industrial waste was presented for the first time.